Appendix E

Hydrology Reports, Phase 1 and Phase 2

1005 O'BRIEN DRIVE Preliminary Hydrology Report Phase 1

February 8, 2022 Revised: March 8, 2022 C20181310

> PREPARED FOR: DES Architects + Engineers, Inc. 399 Bradford St. Redwood City, CA

> > On behalf of **Tarlton Properties, Inc.** 1530 O'Brien Dr., Suite C Menlo Park, CA



DESIGN ENGINEER: BKF ENGINEERS 255 Shoreline Drive, Suite 200 Redwood City, CA 94065 Chuck Humpal P.E. CA 53325

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1. INTRODUCTION

Tarlton Properties, Inc. (Tarlton Properties), has proposed redevelopment of three parcels in Menlo Park currently containing three buildings: 985 and 1001 O'Brien Drive and 1320 Willow Road. The buildings are planned to be replaced with a new building identified as 1005 O'Brien Drive, parking garage, and other various site improvements (Project). This is Phase 1 of a planned two-phase project. This report will only consider the improvements and redevelopment occurring within Phase 1.

The purpose of this report is to document the existing drainage conditions in and around the Project property as well as the design of storm water conveyance and management facilities per the City of Menlo Park Drainage Guidelines (City Guidelines).

2. BACKGROUND

Tarlton Properties intends to redevelop the Project site currently containing 985 and 1001 O'Brien Drive and 1320 Willow Road. Location can be seen in Figure 1 below. The project intends to demolish 985 and 1001 O'Brien Drive as well as the east half of the 1320 Willow Road building. The buildings are planned to be replaced with a new building, identified as 1005 O'Brien Drive, as well as new parking garage and storm water treatment.

The adjacent property to the east, 1035 O'Brien Drive, will be slightly modified with a relocated west property line and driveway access into the Project site. The adjacent property to the west, 965 and 935 O'Brien Drive, will remain undisturbed. The west half of the existing property to the northwest, 1320 Willow Road, will remain with a new exterior wall as an interim condition until it is demolished and redeveloped in Phase 2.

The Project site is approximately 3.2 acres and is bound by an improved area directly north of the site. This area consists of a parking lot and playing field adjacent to Mid-Peninsula High School. Record maps indicate that the adjacent improved parcel is partially within the San Francisco Public Utility Commission (SFPUC) / Hetch Hetchy right of way. The site is also bound by existing buildings and Willow Road to the west, O'Brien Drive to the south, and an existing building to the east.

The existing site is composed of existing industrial businesses encompassing a gross floor area of approximately 67,000 square feet, parking areas, and minor landscape features. The existing site is 99% covered with impervious surface. The Project intends to significantly increase the site's pervious area. With the proposed improvements on 1005 O'Brien Drive, approximately 26,080 square feet of new pervious surface will be added. The modified landscape area will include one bio-retention area and one self-treating area to treat run-off from the newly created and replaced impervious areas.



Preliminary Hydrology Report February 8, 2022; Revised March 8, 2022

The Project site is located near the downstream end of the drainage shed noted as the San Francisco Bay drainage basin; based on Attachment A of the City of Menlo Park Requirements for the Preparation of Hydrology Reports (City Hydrology Requirements). The location is outside of the problem areas indicated in Attachment B of the City Hydrology Requirements, thus not requiring hydrograph modifications. Both attachments are included in Appendix A of this report. The site is not connected to any of the storm drainage systems analyzed as a part of the May 2003 City-wide Drainage Study. Therefore, it is assumed the system that this site's storm drain will outlet to has no capacity issues.

The current Federal Emergency Management Agency (FEMA) base flood elevation (BFE) for the site was determined to be between elevations 12 to 13 (NAVD 88) based on the Federal Emergency Management Agency Insurance Rate Map dated April 5, 2019. The flood elevation was interpolated to be 12.8. The site is located within Zone AE which is indicated as a Special Flood Hazard Area. The currently available FEMA Insurance Rate Map is attached as Figure 7. The proposed finished grades for the project range between elevations 12.50 at the lowest connection to the existing condition and 14.80 as the finished floor of both the proposed building and garage. Therefore, the finished floors of the buildings and the garage will be 2 ft above the BFE. Note that the BFE is the flood elevation that will occur during a 100 year storm event. All elevations presented in this report are NAVD 88.



Figure 1: Vicinity Map



3. EXISTING CONDITION

The regional drainage pattern in the vicinity of the Project site appears to be from south to north. The project site itself does not have a known underground storm drain system but instead uses overland flow to direct the majority of the storm water run-off to a long valley gutter system internal to the property. The on-site storm water is collected via the valley gutter and drained from the south and west toward and outfalls to an off-site existing inlet near the northeast corner of the property. Run-off for the site ultimately drains to a 48-inch storm drain line located west of 1315 O'Brien Drive. The existing conditions for the site and immediate area can be seen in the attached Figure 3.

3.1 ON-SITE DRAINAGE

As stated above, the site does not have a known underground storm drain system. A survey performed by Kier+Wright indicates an on-site catch basin, noted as a drywell with no outlets. Therefore, it is assumed that run-off from the existing roof water leaders is discharged directly to the hardscape surface where it and the other storm water discharge collect in the valley gutter. The site relies almost completely on overland flow to discharge storm water to the receiving inlet. Currently, there are no known storm water management facilities on-site that provide treatment or detention.

3.2 OFF-SITE DRAINAGE

Topographic information indicates that, except for minor losses around the edges of the properties, the site's drainage remains on-site until it flows to the outfall. Off-site drainage immediately around the Project site is limited to overland flow along O'Brien Drive's gutter system and overland flow onto the SFPUC's parcel.

Off-site drainage immediately around the Project site is limited to overland flow along O'Brien Drive's gutter system. The gutter system conveys stormwater from the site, as well as other properties bordering the street, east to the nearest public storm drain catch basins at the intersection of Kelly Court and O'Brien Drive. From there, storm water is conveyed through the City's storm drain system to eventually discharge to the SFPUC parcel and eventually flows to a 48-inch storm drain line west of 1315 O'Brien Drive, northeast of the Project. The adjacent parcel, to be developed in Phase 2, as well as those properties immediately west of the site, currently drain to Willow Road and are picked up by the existing 66-inch storm drain therein. Flow through the 66-inch Willow Road storm drain line is part of a separate system and does not appear to receive tributary flow from the Phase 1 project site. Nevertheless, both the 48 and 66 -inch lines ultimately discharge to the San Francisco Bay.

A significant portion of the off-site drainage area for the 48-inch line lies within East Palo Alto's jurisdiction. Off-site drainage to the 48-inch line was approximately delineated only for the purpose of visualizing a reasonable tributary area. It is not intended to provide a detailed analysis of off-site system and drainage pattern. Refer to the attached Figure 2 for the off-site drainage area delineation map.



4. BASIS OF DESIGN

The following summarizes the basis of design for the corresponding calculations found in the attached Tables 2 and 3.

Determination of site design flow rates are based on the Rational Method: The Rational Method is defined as Q = C I A, where:

- Q = peak flow (cfs)
- C = run-off coefficient
- I = rainfall intensity (in/hr)
- A = area (acres)

Design Storm Event: The storm drain system is evaluated for a 10-year storm event.

Time of Concentration: For this report, on-site time of concentration is assumed to be 10 minutes.

Run-off Coefficient: Run-off coefficients are developed using the City of Menlo Park Requirements for the Preparation of Hydrology Reports (August 20, 2006). Run-off coefficient of 0.95 was used for all impervious areas. Run-off coefficient of 0.3 was used for all pervious and landscaped areas based on the upper limit of the Coefficient of Run-off chart provided within the City Hydrology Requirements. A weighted run-off coefficient of 0.944 and 0.821 were calculated and implemented for the existing and proposed coefficients, respectively.

Rainfall Intensity: The rainfall intensity for the 10-year design storm event was calculated using Attachment C - Menlo Park IDF Curve.

Freeboard: The existing system is evaluated against the 10-year event contained within the storm drain system.

Rim Elevations: Rim elevations are based on a combination of the DES Architects+ Engineers (DES) grading plan and the topographic survey for the site.



5. PROJECT IMPROVEMENTS

Tarlton Properties intends to demolish two and a half existing buildings over three parcels and redevelop the property to contain an office building, parking structure, and landscaping. The existing buildings on the parcels are proposed to be demolished, with the notable exception of the west half of the 1320 Willow Road building, which will receive a new exterior wall and remain standing until being demolished in Phase 2.

With the proposed improvements, the Project is anticipated to add 26,082 square feet of new pervious surface. The Project will also be replacing 111,026 square feet of impervious surface; and proposes to meet storm water treatment requirements by directing run-off from uncovered parking area and/or driveways onto vegetated areas, minimize impervious surfaces, provide self-treating areas, and provide a bio-treatment basin.

As can be seen in Figure 5: Preliminary Stormwater Management Plan, the bio-retention basin area, SWTM 1, will be located on the south side of the lot. Storm water will enter SWMT 1 via two bubble-up structures, one on either end of the basin, each with an outlet elevation of 12.00. A maximum ponding elevation of 11.75 is noted on Figure 6: Preliminary Utility Plan. If the storm water level exceeds elevation 11.75, it will be directed into the FTP's downstream overflow structure, bypassing the media filtration. SWTM 2 is located on the north end of the lot and is self-treating. Storm water will flow north and be intercepted by a French drain along the northern boundary line.

Storm water is collected via overland flow which directs it to a network of proposed storm drain lines accessed by multiple catch basins throughout the property. The storm water is then channeled to the basin on the south side of the property. After traversing the basin, storm water ultimately drains to a lift station at the northeast corner of the property. Likewise, the stormwater entering collected by the French drain from SWMT 2 will be conveyed to the lift station. The lift station will be equipped with a low-flow pump to lift the storm water up to the surface where it will then flow overland across the property into the existing catch basin just north of the property, mimicking the existing flow pattern of the valley gutter system. The design of the proposed drainage system is depicted in Figure 4: Preliminary Grading Plan and Figure 6: Preliminary Utility Plan. Proposed functions of the pump are intended to remove stormwater from the proposed storm drain pipes and structure during low flow scenarios. During high flow situations, the water will bypass the pump and exit the structure as described above. Additional pump details and functions are described in Section 5.2 of this report.



5.1 STORMWATER MANAGEMENT

The Project will create or replace approximately 111,026 square feet of impervious area and convert 27,400 square feet of existing impervious surface to pervious surface. See Table 1: Existing vs Proposed Area Summary below for the changes regarding existing and proposed allocations of impervious and pervious areas.

Per the San Mateo Countywide Water pollution Prevention program (SMCWPPP) C.3 Stormwater Handbook, "Projects that create and/or replace 10,000 square feet or more of impervious surface must comply with Provision C.3". The proposed improvements meet this threshold, and therefore qualifies as a Regulated Project and must include treatment measures.

The footprint of SWTM 1, 4,440 square feet, is approximately 4% of the total proposed and replaced impervious area. Additionally, the project intends to provide 7,820 square feet of pervious self-treating area. Pervious and impervious areas are tabulated on the attached Figure 5: Preliminary Stormwater Management Plan.

	Area (ft²)				
	Existing Proposed Delt				
Impervious	137,108	111,026	-26,082		
Pervious	1,318	27,400	+26,082		
Total	138,426	138,426	0		

Table 1: Existing vs Proposed Area Summary

To meet C.3 requirements, the aforementioned SWMT 1 treatment basin is sized based on the 4% rule for new or replaced impervious area. SWMT 1 and 2 are intended to capture and treat run-off from all 111,026 square feet of impervious area on site. Refer to Figures 4 through 6 for an overview of the proposed drainage system.

The Menlo Park Impervious Area Worksheet prepared by DES is provided under Appendix B of this report. The SMCWPPP C.3 checklist will be provided by DES under a separate submittal with the Stormwater Management Plan.



5.2 PUMP DESIGN

A low flow pump will be installed in the lift station, indicated on the northeast corner property, as seen in Figure 6: Preliminary Utility Plan. A 1/3 horsepower automatic pump with a 2-inch discharge pipe and multiple mechanical float switches will be utilized. The pump shall be a Goulds 2WD Submersible 2" Non-Clog Pump, or approved equal. Further specifications can be seen in Appendix C: Pump Specifications. Per the current development plans, the pump will need to lift the stormwater approximately 6 feet, to the outlet elevation of 11.50. The pump floats will need to be programmed by the manufacturer and installed by the contractor to switch on when the water level rises above elevation 6.20, or 8 inches above the lift station's invert, assuming the invert in of the storm drain pipes is the same elevation as the lift station's invert. If not, the contractor will need to adjust the inverts accordingly. The pump shall continue to run until the water level reaches an elevation 8 inches above the lift station's invert elevation. The floats will be required to be programmed to switch the pump off when the stormwater level in the structure drops below that elevation. This will allow the pump to function properly and minimize the amount of ponding water within the structure. The lift station should incorporate weep holes in the bottom of the structure in order to ensure the remaining water in the base can dissipate after the pump shuts off.

As stated previously, the proposed functions of the pump are only intended to remove stormwater from the proposed storm drain pipes and lift station structure during low flow scenarios. During high flow situations, the water will bypass the pump and exit the structure through the outfall pipe at outlet elevation 11.50.

A control panel for the pump shall be programmed to alert the owner when the pump is active and running normally, when pump is triggered "on" but no movement is recognized, and/or a malfunction has occurred.

The proposed pump shall only function while storm water in the structure is at an elevation 8 inches or more above the lift station's sump invert. Contractor shall construct the structure and device to ensure that the float switches will recognize the correct elevations in order for the water level to always cover the pump impeller during "on" functions. Failure to do so will break suction at the bottom of the pump, introducing air to the system resulting in pump cavitation.

5.2 DETENTION FACILITIES

The City Guidelines require an on-site retention (or detention where retention is impracticable) device if a project increases run-off to the public storm drain system during a 10-year storm event. As shown in Tables 2 and 3, the existing discharge is estimated to be 5.06 cubic feet per second (cfs) and the proposed site discharge is estimated to be 4.41cfs. The reduction is due to the addition of 26,082 square feet of new pervious area. Therefore, the total amount of run-off produced to the public storm drain system will be reduced, and the Project will not need to implement a retention or detention device. As stated, the Project will, however, install one bio-treatment basin and self-treating pervious area to conform to C3 guidelines.



6. STORM DRAIN ANALYSES

The proposed system will collect run-off from the proposed impervious area and convey it to the SWMT 1 and 2. After passing through the SWMT areas, the storm water will ultimately exit the site via a pump conveying the discharge to an off-site inlet, mimicking the existing condition. Based on a review of the existing conditions, it appears that the entire on-site system ultimately conveys storm water to an existing off-site 12-inch collector pipe. This pipe was recently cleaned and inspected via a video camera to confirm its outlet point. This is represented in the topographic survey for 1340 Willow Road shown in Figure 3: Existing Conditions. See Figure 6: Preliminary Utility Plan for the proposed on-site system layout.

Preliminary calculations of the system performed by DES, shown in attached Tables 2 and 3, indicate that the existing discharge for a 10-year storm to the off-site system is approximately 5.06 cfs. The proposed discharge for a 10-year storm to the off-site system was calculated to be 4.41 cfs. These values were calculated using the City Guidelines. The proposed discharge is expected to be less than the existing discharge, therefore, no adverse effects to the existing off-site system are anticipated.

7. CONCLUSION

The existing Project site is served by overland flow to a valley gutter system internal to the property. The valley gutter discharges to an off-site inlet, near the northeastern corner of the property. Currently there are no known storm water management facilities on-site that provide treatment or detention. The discharge of the existing system was estimated to be 5.06 cfs.

The proposed Project improvements include transforming the existing buildings and paved lot on the property to a new office building, parking garage, bio-retention basin and landscaping.

With the proposed improvements, the Project is anticipated to add 26,082 square feet of new pervious surface and create or replace a total of approximately 111,026 square feet of impervious surface. As a result of the increase in pervious surface, the proposed discharge will decrease to 4.41 cfs.

To meet C.3 requirements, the Project proposes to implement one bio-retention basin, equal in area to approximately 4% of the new and replaced impervious area, as well as self-treating landscape area to capture and treat run-off. The basin will be located on the south side of the Project site. After flowing through the basin, the water will discharge to the off-site system, either via gravity or the proposed pump.

The existing off-site system has no known capacity issues, and with the reduction in total discharge from the site, no adverse effects to the existing system are expected.



8. REFERENCES

California Regional Water Quality Control Board, San Francisco Bay Region, Municipal Regional Stormwater NPDES Permit, November 28, 2011

City of Menlo Park City-wide Drainage Study, May 2003

City of Menlo Park Commercial, Multi-Family and Subdivison Grading & Drainage Guidelines, 2020

City of Menlo Park Impervious Area Worksheet, 2020

City of Menlo Park Requirements for the Preparation of Hydrology Reports, August 20, 2006.

Federal Emergency Management Agency insurance Rate Map, October 2012

Kier + Wright Topographic Surveys for 1320 Willow Road, 1001-1015 O'Brien Drive, 985 O'Brien Drive, Dated February 2021

Kier + Wright Topographic Surveys for 1340 Willow Road, Dated November 2021

Kier + Wright ALTA / ACSM Land Title Surveys for 1320 Willow Road and 1001-1015 O'Brien Drive, 985 O'Brien Drive, Dated September 2015

Kier + Wright ALTA / ACSM Land Title Surveys for 985 O'Brien Drive, Dated November 2015

San Mateo County C.3 and C.6 Development Review Checklist, January 2019

San Mateo County, C.3 Regulated Projects Guide, Version 1.0., January 2020.



TABLES

PRELIMINARY ON-SITE DISCHARGE CALCULATIONS FOR PHASE 1 1005 O'BRIEN DRIVE

 DES ARCHITECTS+ ENGINEERS

 399 BRADFORD, SUITE 300

 REDWOOD CITY, CA 94063

 Date
 11/24/2021

 P#
 10025.002

 Source:
 "Requirements for the Preparation of Hydrology Reports" by Menlo Park Public Works (August 2006)

 LAND USE:
 Office Bldg, Parking Garage

 RUNOFF "C":
 0.95(Conc/AC/Roof), 0.30(Landscape)

 Rainfall Intensity 10yr
 Per Attachment C - Menlo Park IDF Curve

Time of Concentration: Initial Tc is assumed to be10 min.

Total Runoff Q for 10-year is calculated using the Rational Formula (Q=CIA)

Existing Onsite Discharge Summary

Existing On-Site Runoff Coefficient Calculation Summary

Type of Surface	Crunoff	Area (ft ²)	Weight			
Impervious	0.95	137,108	130,253			
Pervious	0.3	1,318	395			
	Total	138,426	130,648			
Total Existing Site Composite Run-off C = 0.944						

On-Site Discharge Calculation Summary Q=CIA

Area SF	Area acres	Comp. ^{Coef.} C	СА	Total TIME (MIN.)	INTENSITY II0-yr (IN/HR)	DES. Q (CFS)
138,426	3.178	0.944	3.00	10.00	1.69	5.06

PRELIMINARY ON-SITE DISCHARGE CALCULATIONS FOR PHASE 1 1005 O'BRIEN DRIVE

 DES ARCHITECTS+ ENGINEERS

 399 BRADFORD, SUITE 300

 REDWOOD CITY, CA 94063

 Date
 11/24/2021

 P#
 10025.002

Proposed Onsite Discharge Summary

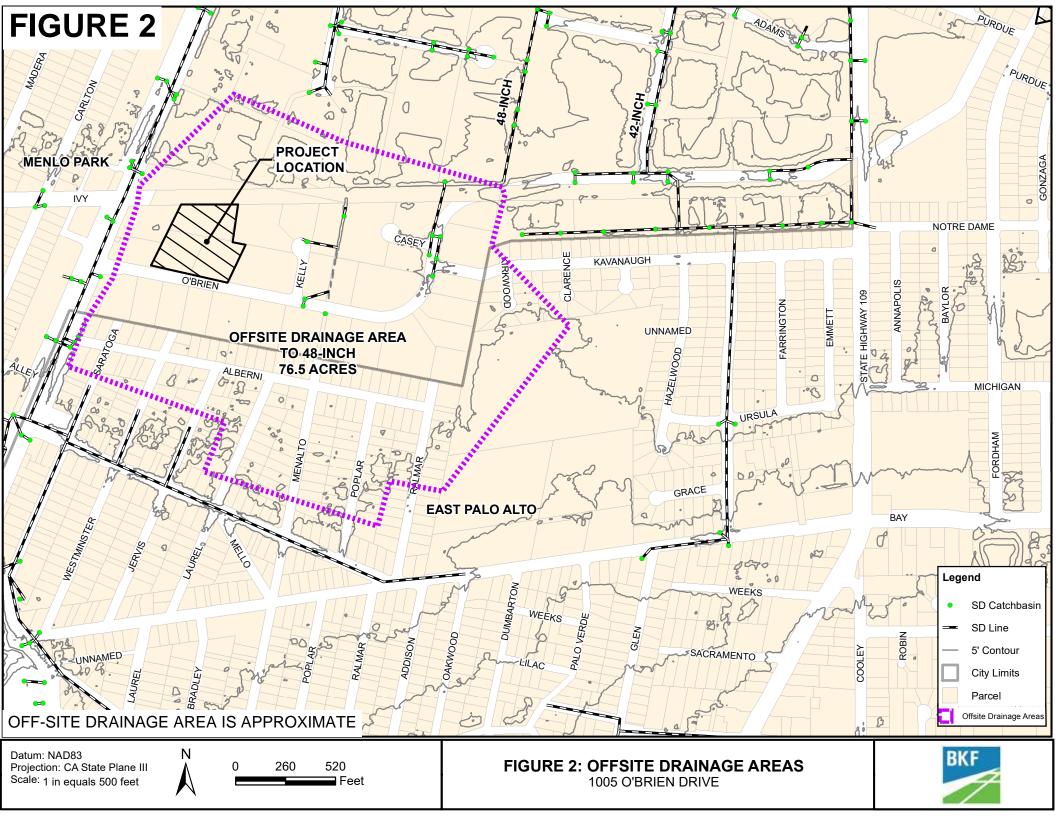
Existing On-Site Runoff Coefficient Calculation Summary

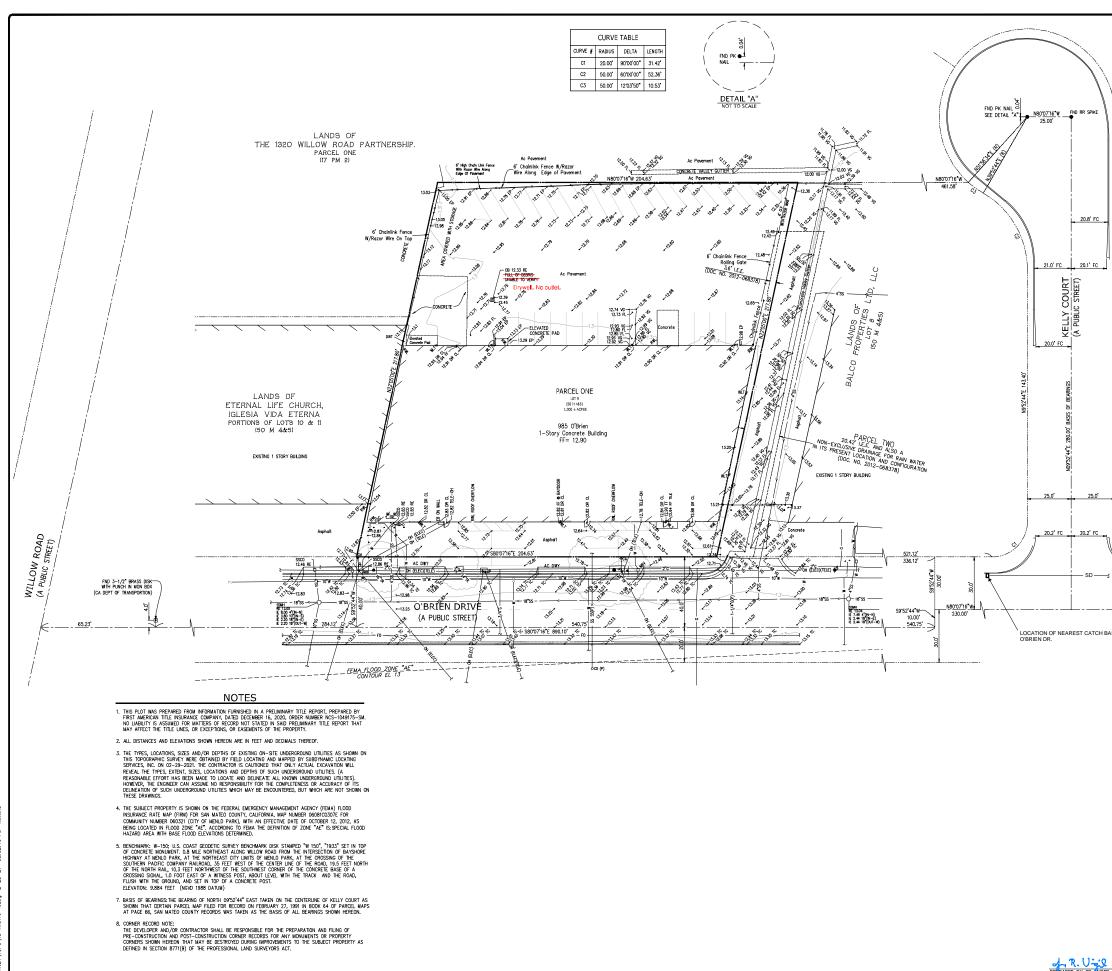
Type of Surface	Crunoff	Area (ft ²)	Weight			
Impervious	0.95	111,026	105,475			
Pervious	0.3	27,400	8,220			
	Total	138,426	113,695			
Total Existing Site Composite Run-off C = 0.821						

On-Site Discharge Calculation Summary Q=CIA

Area SF	Area acres	Comp. ^{Coef.} C	CA	Total TIME (MIN.)	INTENSITY I10-yr (IN/HR)	DES. Q (CFS)
138,426	3.178	0.821	2.61	10.00	1.69	4.41

FIGURES



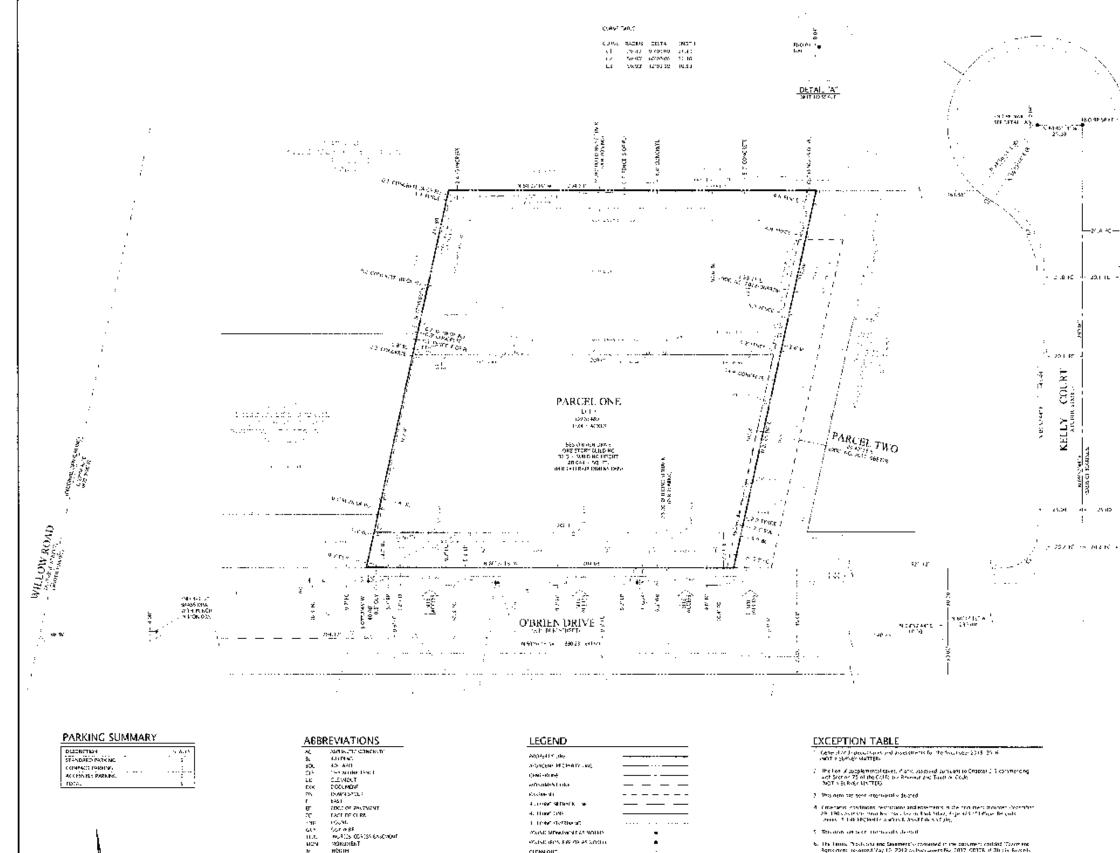


- **EXISTING CONDITIONS** က FIGURE

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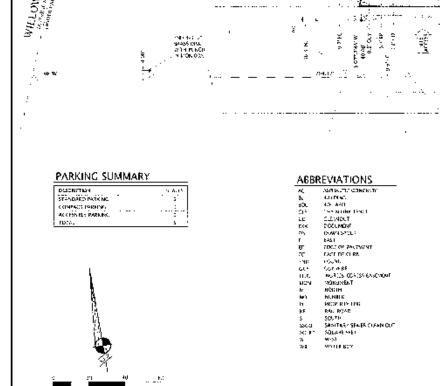
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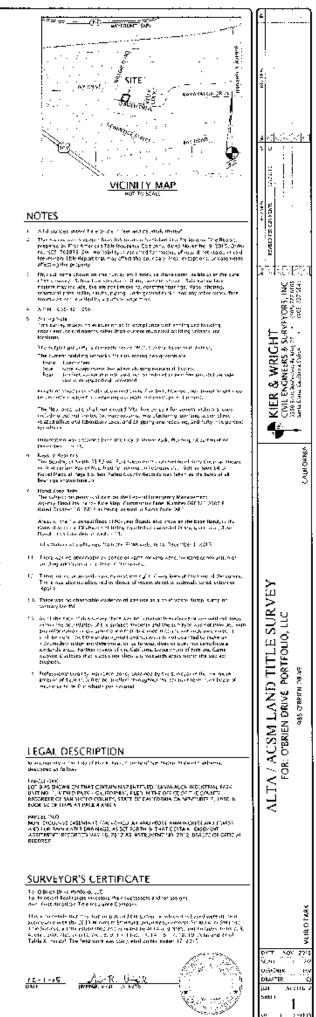


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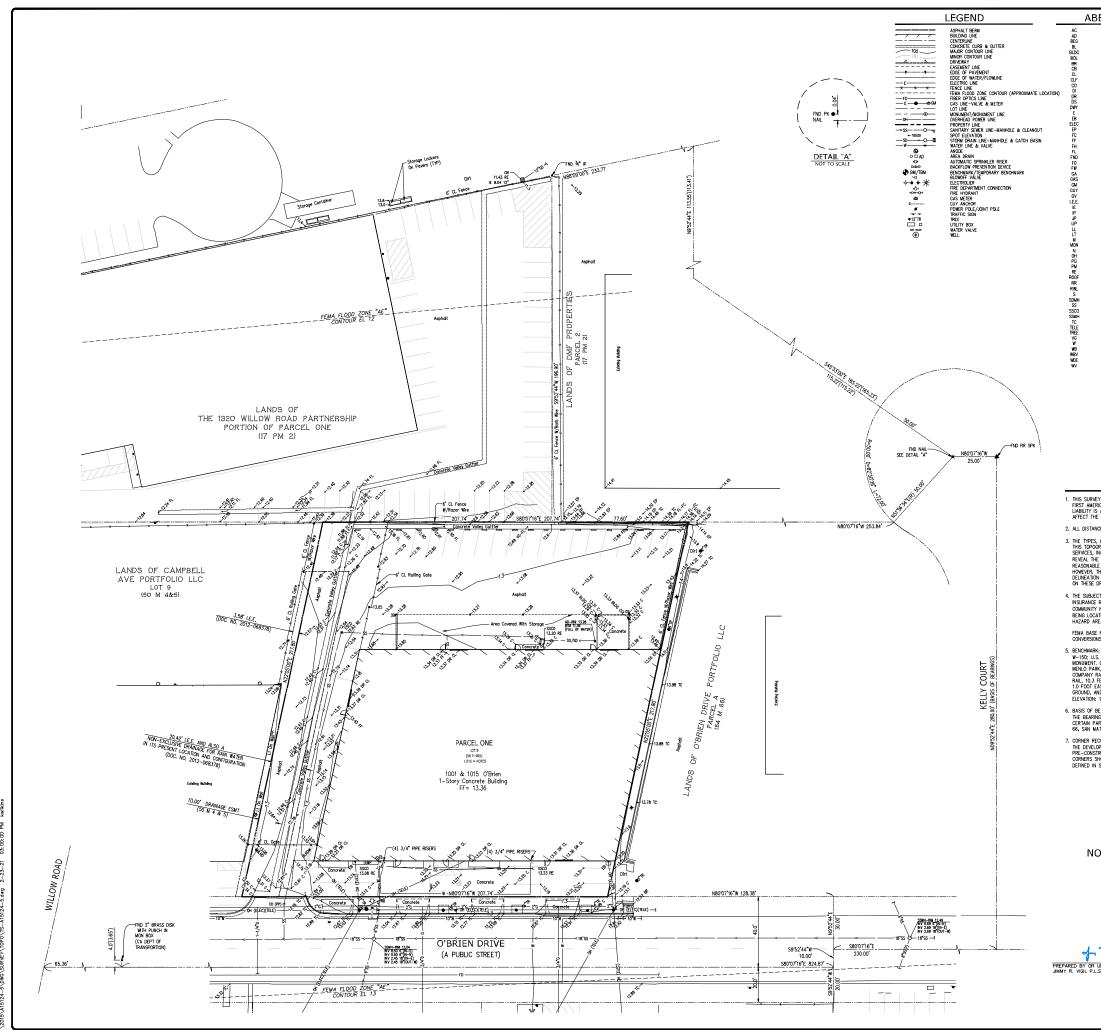
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ABBREVIATIONS

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NOTES

1. THIS SURVEY WAS PREPARED FROM INFORMATION FURNISHED IN A PRELIMINARY ITLE REPORT, PREPARED BY FIRST AMERICAN TITLE INSURANCE COMPANY, DATED DECEMBER 17, 2020, ORDER NO. NCS-1049174-5M. NO LUABULTY IS ASSUMED FOR MATTERS OF FEORD MOT STATED IN SAD PRELIMINARY ITLE REPORT THAT WAY AFFECT THE TITLE LINES, OR EXCEPTIONS, OR EASEMENTS OF THE PROPERTY.

2. ALL DISTANCES AND ELEVATIONS SHOWN HEREON ARE IN FEET AND DECIMALS THEREOF.

3. THE TYPES, LOCATIONS, SIZES AND/OR DEPTHS OF EXISTING ON-STEE UNDERGROUND UTLITES AS SHOWN ON THIS TOPOGRAPHIC SURVEY WERE OFFINED BY FIELD LOCATING AND MAPPED BY SUBDYMARU LOCATING SERVICES, INC. ON 2-29-20-2011 THE CONTRACTOR IS CAUTIONED THAT ONLY ACTUAL EXCAVATION WILL REVEAL THE TYPES, EXTENT, SIZES, LOCATIONS AND DEPTHS OF SUCH UNRERGROUND UTLITES, (A REASONABLE FYORT HIS DEPENDENT AND CENTRAL TAND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE FYORT HIS DEPENDENT AND CENTRAL TAND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE FYORT HIS DEPENDENT AND CENTRAL TAND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE STORT HIS DEPENDENT AND CENTRAL TAND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE STORT HIS DEPENDENT AND CENTRAL TAND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE STORT HIS DEPENDENT AND CENTRAL AND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE STORT HIS DEPENDENT AND CENTRAL AND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE STORT HIS DEPENDENT AND CENTRAL AND OS LINEATE AL KIXOWI NONGROUND UTLITES, (A REASONABLE STORT HIS DEPENDENT AND CENTRAL AND OS LINEATE AL KIXOWI NONGROUND UTLITES) HORINER, THE CONDICER CAN ASSURE NO RESPONSIBILITY FOR THE COMPLETENESS OR ACCURACY OF ITS DELINEATION OF SIGHT UNDERGROUND UTLITES WHICH MAY BE ENCONTERED, BUT WHICH ARE NOT SHOWN ON THESE DRAWINGS.

4. THE SUBJECT PROPERTY IS SHOWN ON THE FEDERAL EMERGENCY MANAGEMENT AGENCY (FEMA) FLOOD INSURANCE RATE MAP (FIRM) FOR SAM MATED COUNTY, CALICORMA, MAP NUMBER 06081C0307E FOR COMMUNITY MUMBER 060321 (CITY OF MENLO PARK), WITH AN FERENTIE DATE OF COTORET 12, 2012, AS BEING LOCATED IN FLOOD ZONE "AC", ACCORDING TO FEMA THE DEFINITION OF ZONE "AC" INSSPECIAL FLOOD HAZARO AREA WITH BASE, FLOOD ELEVITIONS DETERMINED.

FEMA BASE FLOOD ELEVATIONS ARE BASED ON NAVD88 DATUM. SEE BENCHMARK NOTE FOR DATUM CONVERSIONS.

SENCHAMAR: W-150, U.S. COAST GEODETIC SURVEY BENCHMARK DISK STAMPED *W 150°, *1933* SET IN TOP OF CONCRETE MOMULENT IS MILE NORTHEAST ALONG WILLOW ROAD FROM THE INTERSECTION OF BAYSIORE HIGHWAY AT MENLO PARK, AT THE NORTHEAST CIT LIMITS OF MENLO PARK, AT THE CROSSING OF THE SOUTHENN PACINE COMPARY FARMENDAL SS FEET WAST OF THE CONTRICT LIMITS OF MENLO PARK, AT THE CROSSING OF THE SOUTHENN PACINE COMPARY FARMENDAL SS FEET WAST OF THE CONTRICT LIMITS OF MENLO PARK, AT THE CROSSING OF THE SOUTHENN PACINE COMPARY FARMENDAL SS FEET WAST OF THE CONTRICT LIMITS OF MENLO PARK, AT THE CROSSING OF THE SOUTHENN PACINE COMPARY FARMENDAL SS FEET WAST OF THE CONTRICT LIMITS OF MENLO PARK, AT THE CROSSING OF THE SOUTHENN PACINE TO FOOT EAST OF A WITHESS FOOT, ADDUIT LIVEL WITH THE TRACK AND THE ROAD, PLUEH WITH THE CROWN, NO SS FEN TOP OF CA CONCRETE POST. ELEVATION: 9.884 FEET (NOVD 1988 DATUM)

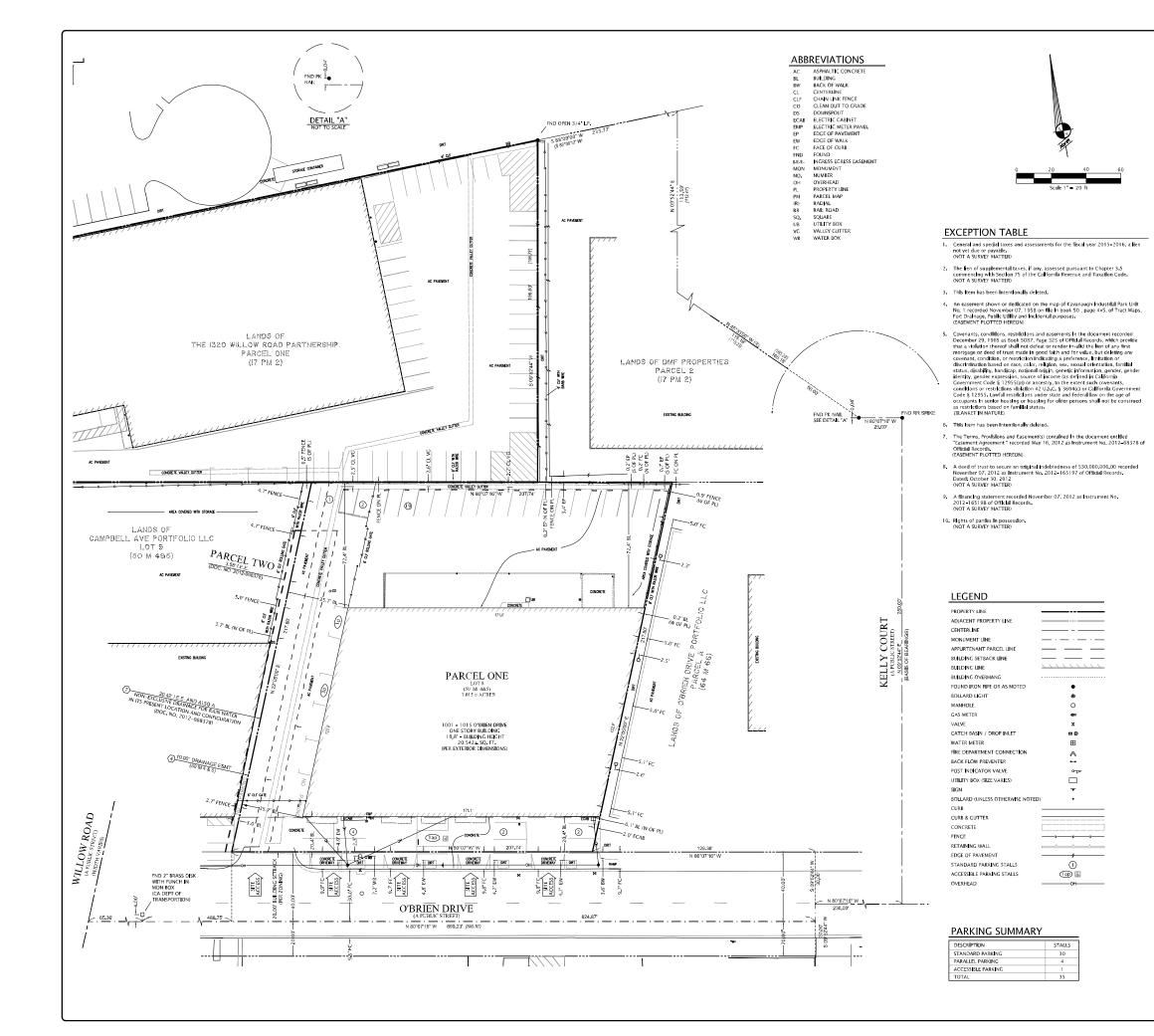
6. BASIS OF BEARING THE BEARING OF NORTH 0952/44" EAST TAKEN ON THE CENTERLINE OF KELLY COURT AS SHOWN ON THAT CERTAIN PARCEL MAP FILED FOR RECORD ON FEBRUARY 27, 1991 IN BOOK 64 OF PARCEL MAPS AT PAGE 66, SAN MATED COUNTY RECORDS WAS TAKEN AS THE BASIS OF ALL BEARINGS SHOWN HEREON.

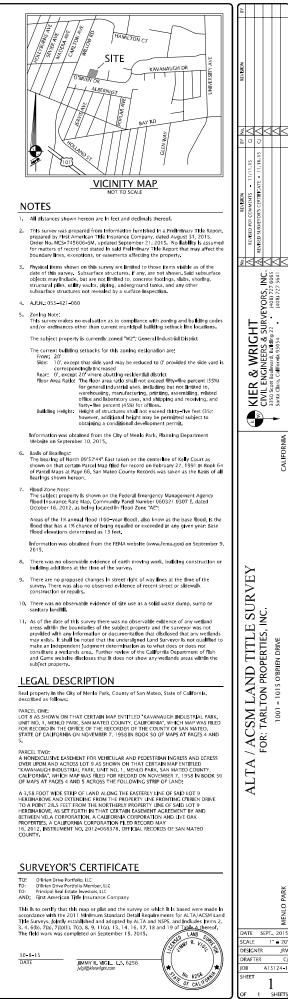
CORNER RECORD NOTE: THE DURLOPER NOTACION CONTRACTOR SHALL BE RESPONSELE FOR THE PREPARATION AND FLUNG OF PRE-CONSTRUCTION AND POST-CONSTRUCTION CORRER RECORDS FOR ANY MONUMENTS OR PROPERTY CORRERS SHOWN HEREON THAT WAT BE DESINGHED DURING IMPROVEDINTS TO THE SUBJECT PROPERTY AS DETINED IN SECTION 577(8) OF THE PROFESSION. LANG SUPERVISE XGT.

NOTE: THIS SITE HAS FIBER OPTIC LINES LOCATED ON OR ADJACENT TO IT.

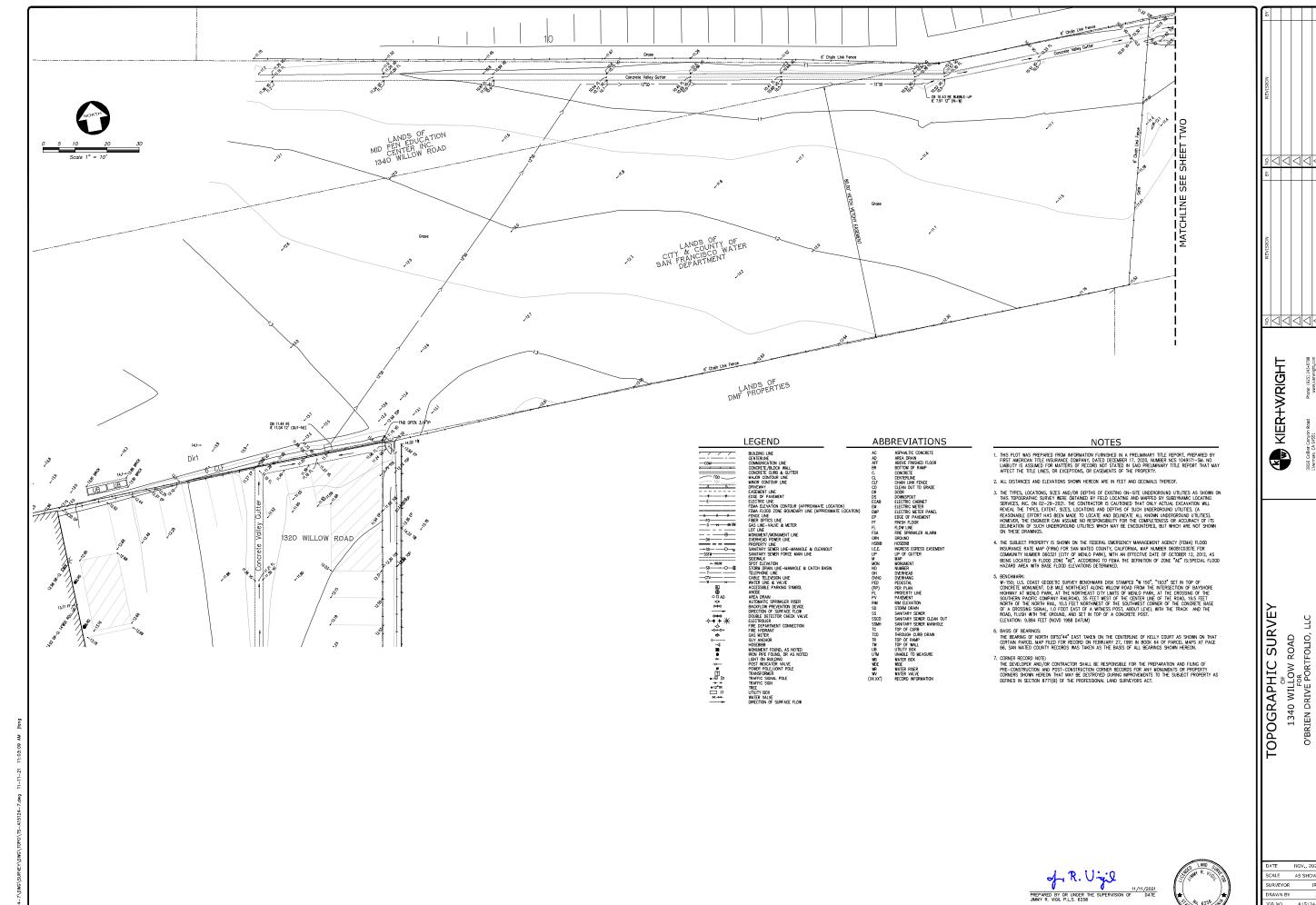
of R. Uije PREPARED BY OR UNDER THE SUPERVISION OF JMMY R. VIGIL P.L.S. 6256





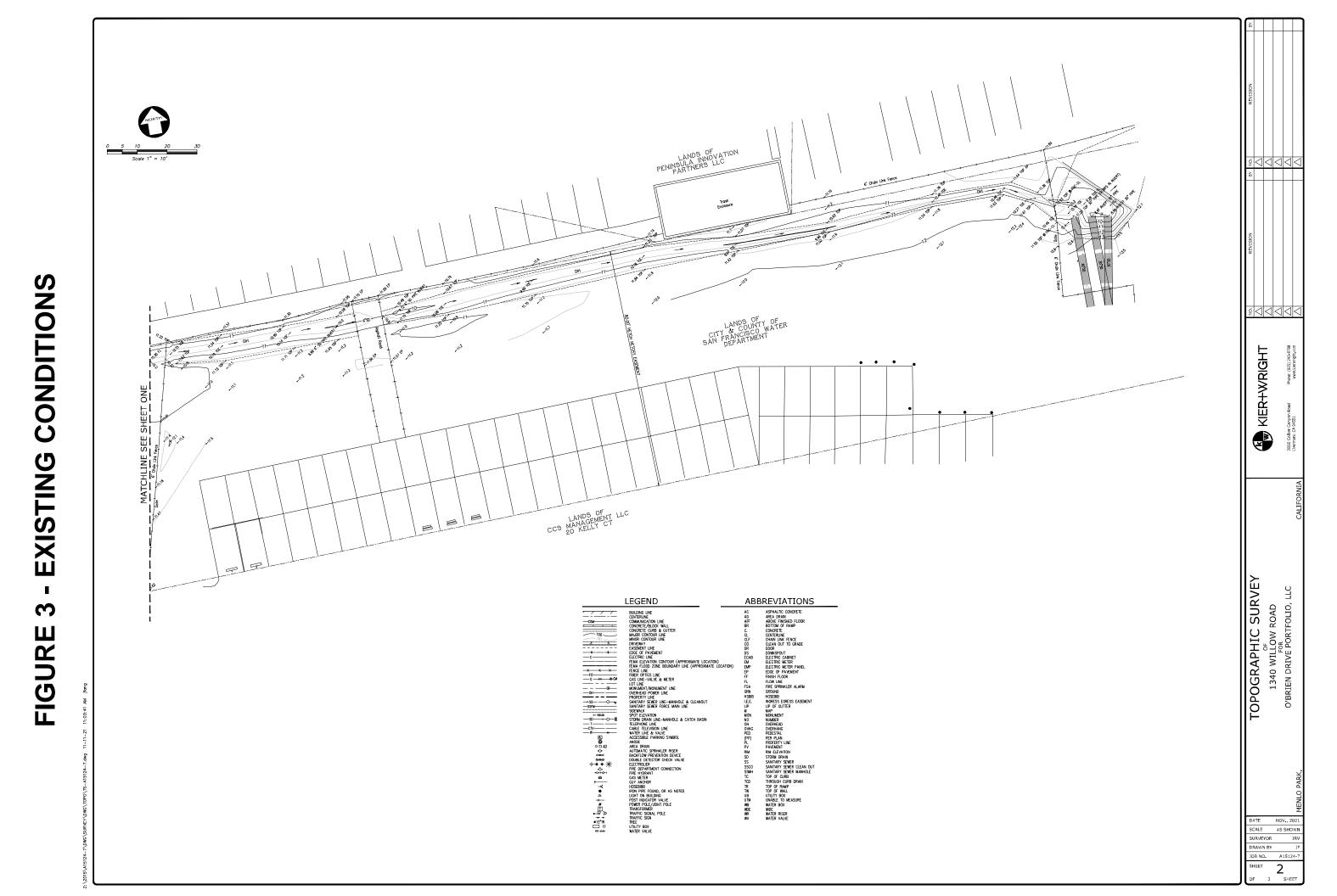


USER-cjunokas E\PROJECTS\A15124-1\DWG\SURVEY\ALTA\C-ALTA.dwg_NOVEMBER16, 2015_9.51 AM

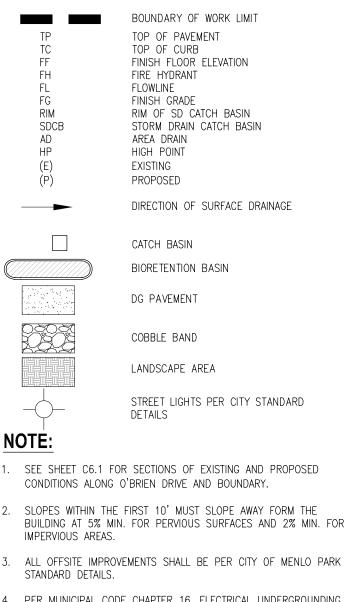


EXISTING CONDITIONS က FIGURE

DATE NOV., 2021 SCALE AS SHOWN SURVEYOR JR\ DRAWN BY JOB NO. A15124-7 SHEET 1 2 SHEET







4. PER MUNICIPAL CODE CHAPTER 16, ELECTRICAL UNDERGROUNDING (LESS THAN 60KV AND COMMUNICATION LINES).

BENCHMARK:

(FROM TOPOGRAPHIC SURVEY PREPARED BY KIER & WRIGHT SURVEYORS: JOB A15124-5 DATED FEB. 2021)

FLOOD ZONE NOTE:

THE SUBJECT PROPERTY IS SHOWN ON THE FEDERAL EMERGENCY MANAGEMENT AGENCY FLOOD INSURANCE RATE MAP, MAP NUMBER 06081C0307E FOR COMMUNITY PANEL NUMBER 060321 0307 E, DATED OCTOBER 16, 2012, WITH THE SITE BEING LOCATED IN FLOOD ZONE "AE";

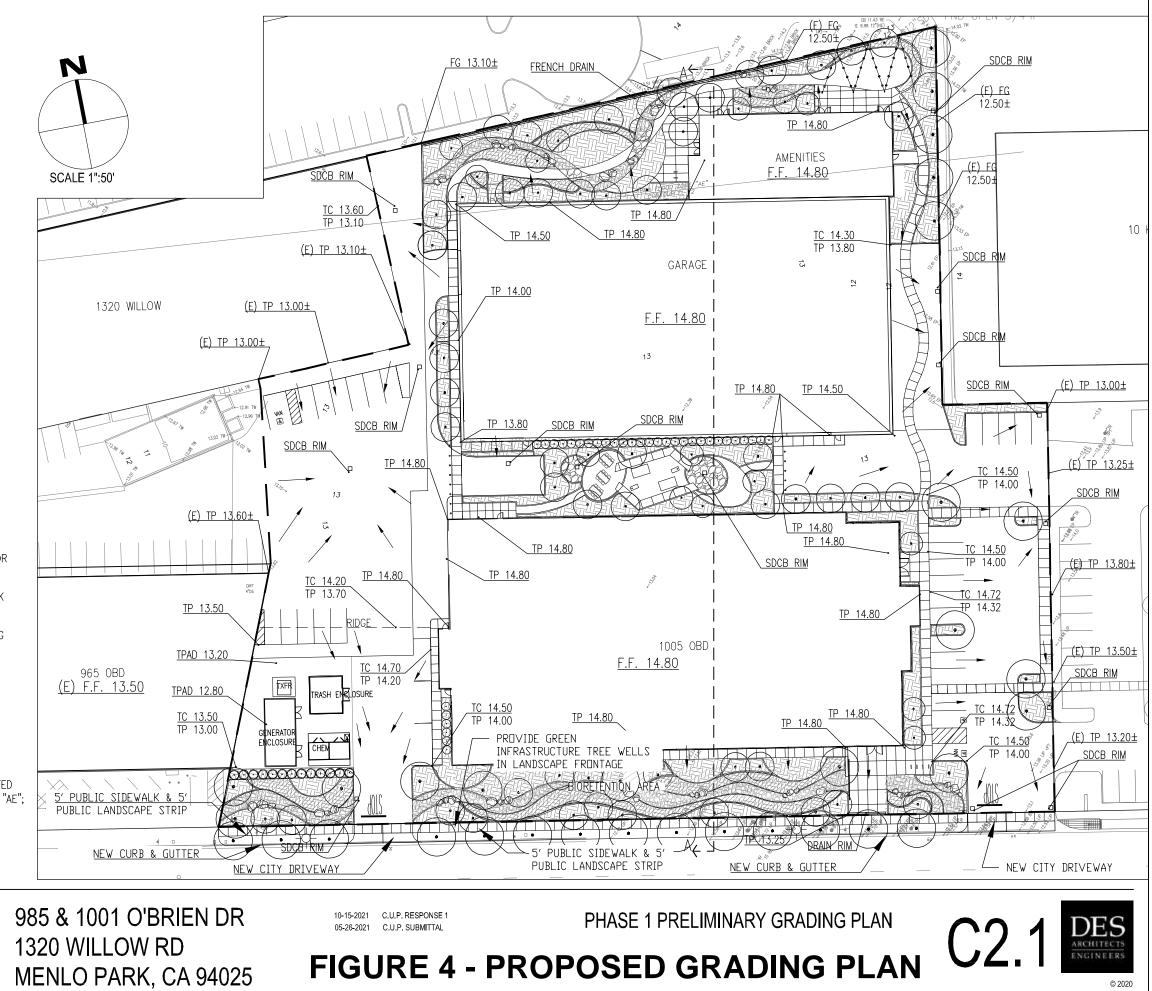
BASE FLOOD ELEVATION DETERMINED AS 12.8 FEET.

NOTE: THE PROJECT WILL BE DESIGNED AND CONSTRUCTED IN COMPLIANCE WITH CURRENT FEMA REGULATIONS AND CITY'S FLOOD DAMAGE PREVENTION ORDINANCE.









2.

3.

SHEET NOTES:

- 1. DIRECT RUNOFF FROM UNCOVERED PARKING AREAS AND/OR DRIVEWAYS ONTO VEGETATED AREAS.
- 2. MINIMIZE IMPERVIOUS SURFACES.
- 3. PROVIDED SELF-TREATING AREAS.
- 4. PRELIMINARY SIZING IS BASED ON THE SIMPLIFIED APPROACH OR FLOW-BASED SIZING APPROACH IN WHICH THE SURFACE AREA OF THE TREATMENT MEASURE IS DESIGNED TO BE 4% OF THE IMPERVIOUS AREA TO BE TREATED.

LEGEND:



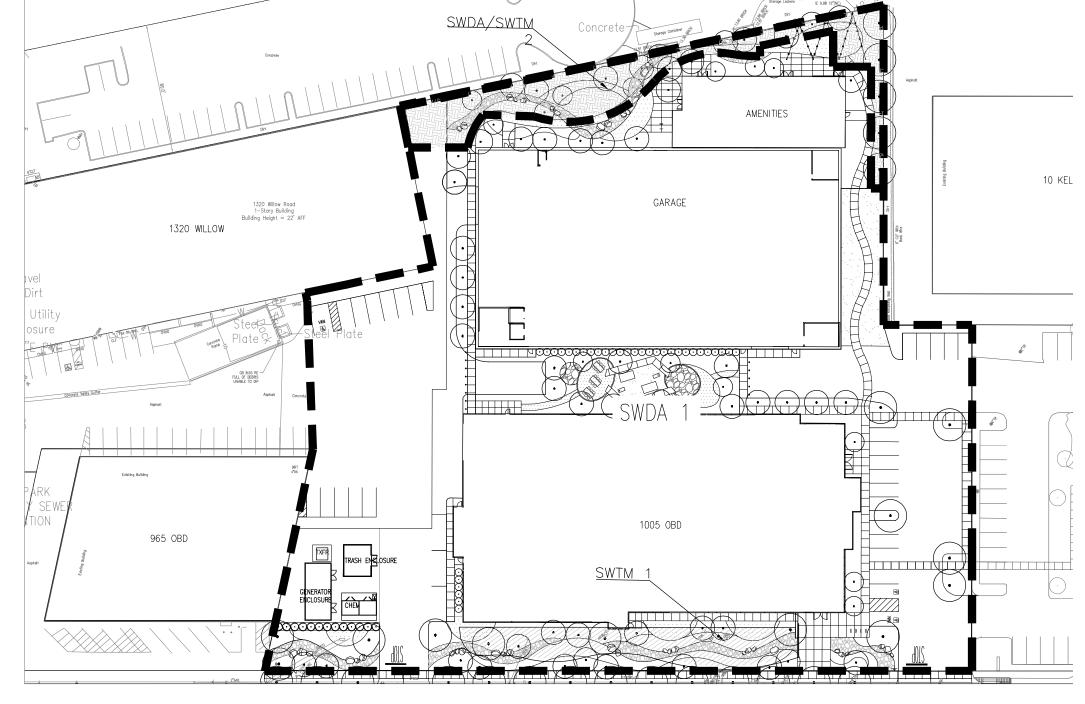
PROPOSED STORMWATER DRAINAGE AREA BOUNDARY BIORETENTION BASIN

SELF TREATING AREA

ABBREVIATIONS:

SWDA	STORMWATER	DRAINAGE AREA
JUDA	STORMARTER	DIVININOL MILLA

SWTM STORMWATER TREATMENT MEASURE



STORMWATER MANAGEMENT TREATMENT MEASURE SUMMARY:

DRAINAGE AREA #	STORMWATER TREATMENT MEASURE	TREATMENT MEASURE DESIGNATION #	TOTAL AREA (SQ. FT.)	IMPERVIOUS AREA (SQ. FT.)	PERVIOUS AREA (SQ. FT)	TREATMENT AREA REQUIRED (SQ.FT.)	TREATMENT AREA PROVIDED (SQ. FT.)
SWDA 1	BIORETENTION AREA	SWTM 1	130606	111026	19580	4440	4440
SWDA 2	SELF-TREATING AREA	SWTM 2	7820	0	7820	N/A	7820

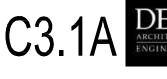


985 & 1001 O'BRIEN DR 1320 WILLOW RD MENLO PARK, CA 94025

PHASE 1 PRELIMINARY STORMWATER MANAGEMENT PLAN

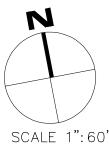
10-15-2021 C.U.P. RESPONSE 1

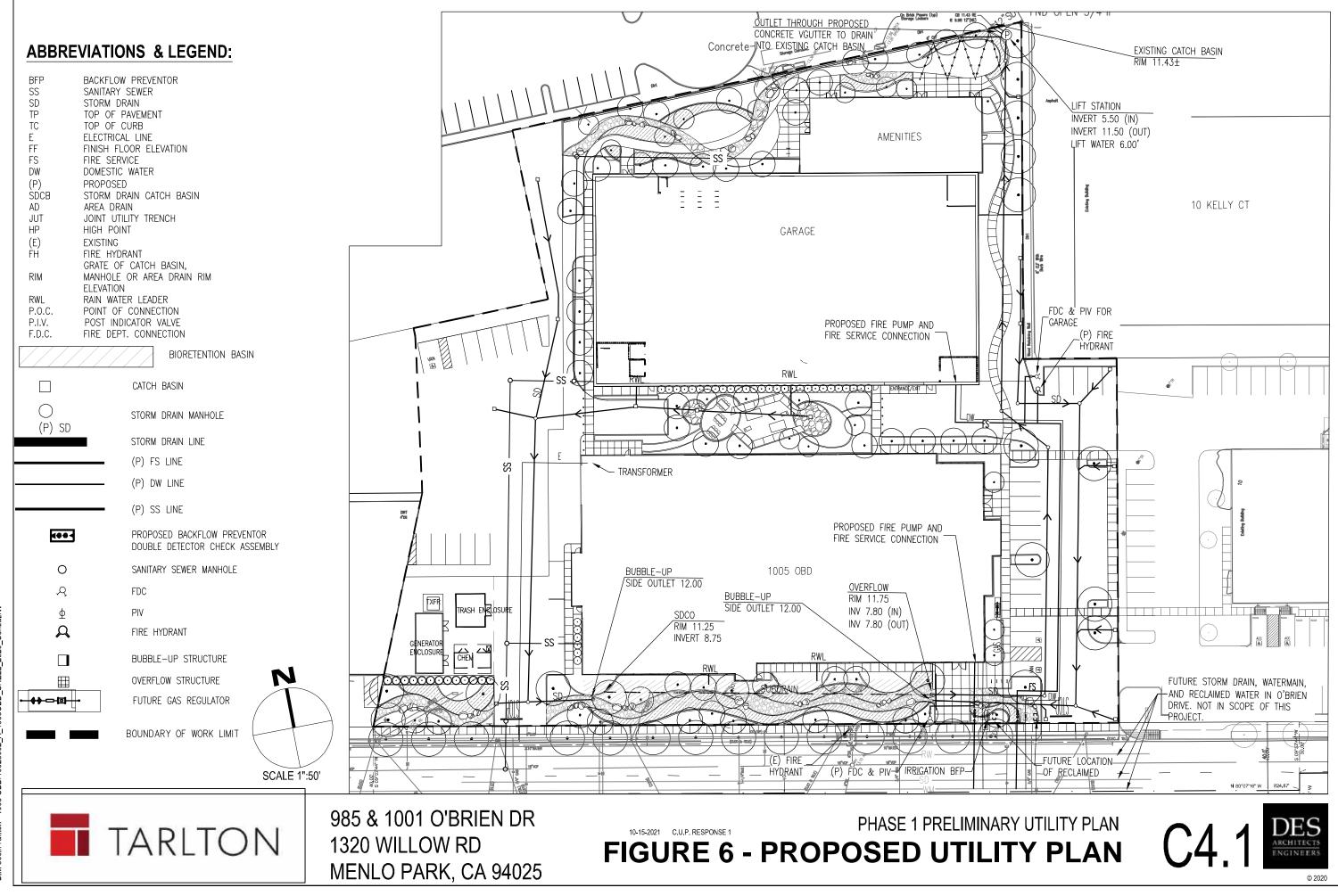
FIGURE 5 - PROPOSED SWMP PLAN







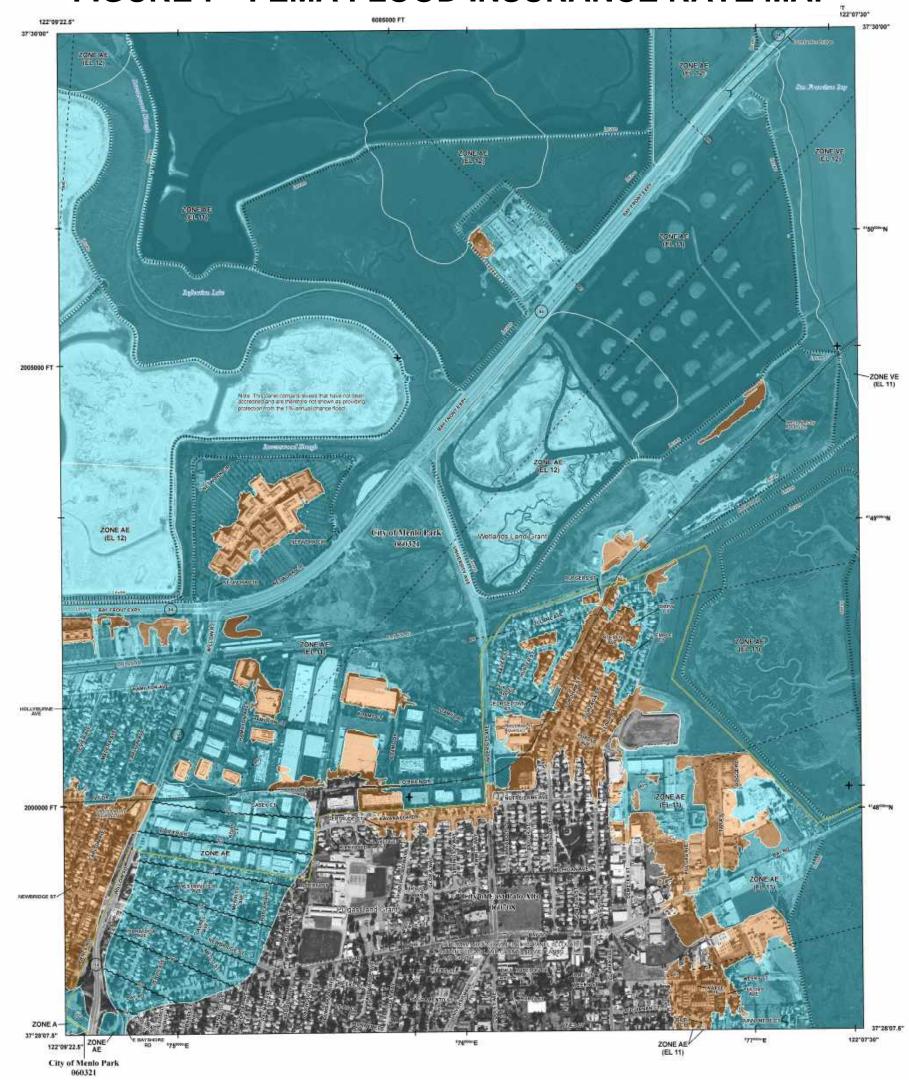




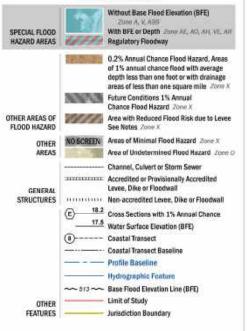
CONDITIONS PROPOSED 4 Ш FIGUR

BIM 360://Tarlton - 1005 OBD/10025002_A_เบบอบอบอากะเ-_2บ2บ_บอกเชลเทข

FIGURE 7 - FEMA FLOOD INSURANCE RATE MAP



SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT THE INFORMATION DEPICTED ON THIS MAP AND SUPPORTING DOCUMENTATION ARE ALSO AVAILABLE IN DIGITAL FORMAT AT HTTPS://MSC.FEMA.GOV



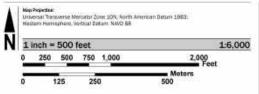
For information and questions about this maps, available products associated with this FEMI instuding feators vertices and this FEMI, this to order centurities at the National Floated Insurance Program in general, passes and the FEMIA Also internation accurate at 1-357-FEMIAM (P1.437:303-2021) unvisit the FEMIA Maps Service Center versile at https://temacilena.gov.available.products.p

ses annexing land on adjacent FIBM panels must obtain a surient copy of the adjacent panel as well rank FIBM Index. These may be ordered directly from the Map Service Center at the number lated.

mywide map stales refer to the Flood insurance Study report for this jurnitiation

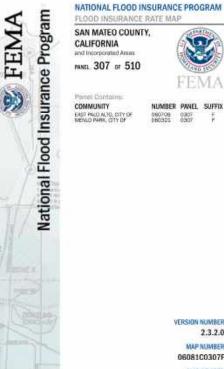
To determine if flood insurance is evaluable in this community, contact your impurance agent or cell the National Hood insurance Program at 1-932-938-9920.

Base map information shown on this FIRM was derived from USGS LIDAR dated 2010 and Coastal California digital insight, stated 2011. USES NAUP imagery dated 2012 is used in anois not covered by the Coastal California sight/imagery.



PANEL LOCATOR





VERSION NUMBER 2.3.2.0 MAP NUMBER 06081C0307F

FEM/

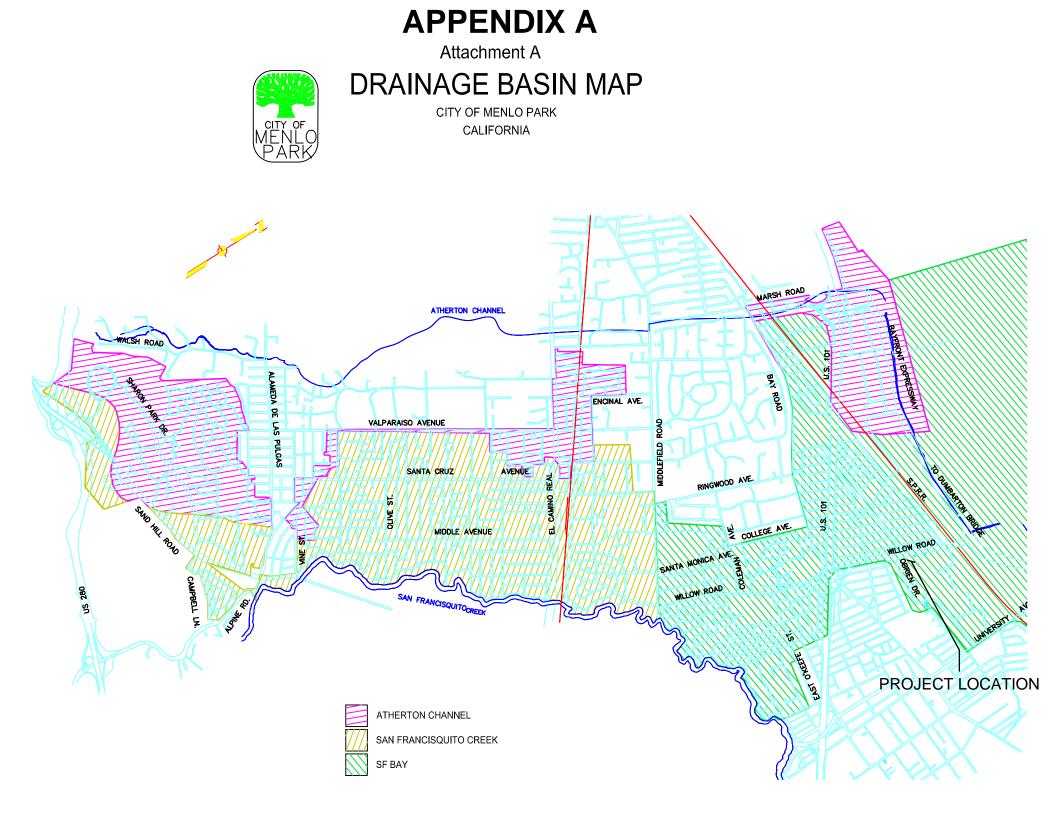
1

NUMBER PANEL SUFFIX

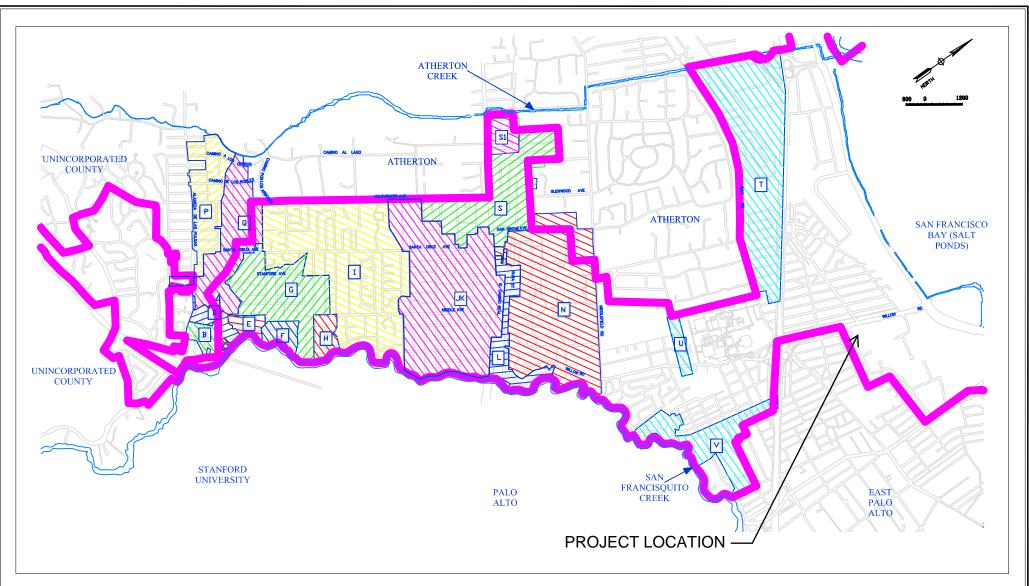
060706 0307 060321 0307

MAP REVISED APRIL 5, 2019

APPENDIX A: MENLO PARK HYDROLOGY REQUIREMENTS ATTACHMENTS A AND B



APPENDIX A





ATTACHMENT B STORM SYSTEM DRAINAGE AREAS MAP

APPENDIX B: CITY OF MENLO PARK IMPERVIOUS AREA WORKSHEET

APPENDIX B

IMPERVIOUS AREA WORKSHEET Page 1

Submit this form with the improvement plan set to the City of Menlo Park Engineering Division.

Date: <u>055421060; 0554210</u> 50; 055421160 Property Address: <u>1005 O'Brien Drive (Phase 1)</u>	APN: 055421060; 055421050; 055421160
Project Description: <u>New Building and Parking Ga</u>	lrage
Contact Name: Elke MacGregor	
Contact Telephone Number: 650-364-6453	
Contact Email: emacgregor@des-ae.com	
Title And Sheet# of Submitted Drawing used For Ca	lculations:
Land Use (Circle One): Residential Commercial Industrial	Professional Roadway
Drainage Basin (Circle One): (See the <i>Hydrology Report Requirements</i> for a D	rainage Basin map <i>.)</i>
Atherton Creek San Francisquito Cree	k San Francisco Bay
I certify that the calculations below accurately refle impervious surfaces for the above project.	ect the proposed changes and final
Calculations Performed By (Print): Max DeAndreis	s, PE
Title: Civil Engine	eer
Calculations Performed By (Signature): John M Date: 11/24/202	aquell Ochahuer

IMPERVIOUS AREA WORKSHEET Page 2

IMPERVIOUS AREA TABLE							
Total Area of Parcel		A <u>138426 ft²</u>					
Existing Pervious Area		B <u>1318</u> ft ²					
Existing Impervious Area		C <u>ft²</u> 137108					
Existing % Impervious	$\frac{C}{A}$ x 100	D <u>99.0</u> %					
Existing Impervious Area To Be Replaced W/ New Impervious Area		E ft ² 109708					
Existing Pervious Area To Be Replaced W/ New Impervious Area		F ft ² 1318					
New Impervious Area (Creating and/or Replacing)* *If greater than 10,000sqft, a hydrology report must be submitted	E + F	G 111026 ft ²					
Existing Impervious Area To Be Replaced W/ New Pervious Area		H_27400 ft ²					
Net Change In Impervious Area ¹	F–H	l -26082					
Proposed Pervious Area	B – I	$\frac{\mathbf{J}}{\mathrm{ft}^2} 27400$					
Proposed Impervious Area* *Verify that J + K = A	C + I	<mark>К</mark> <u>ft²</u> 111026					
Proposed % Impervious	$\frac{K}{A}$ x 100	L <u>%</u> 80.2					

¹ Net change in impervious area is the area required by

APPENDIX C: PUMP SPECIFICATIONS



TECHNICAL BROCHURE

APPENDIX C

B2WD-3WD R3



2WD/3WD

SUBMERSIBLE 2" NON-CLOG SEWAGE PUMP DUAL SEAL WITH SEAL SENSOR PROBE





Goulds Water Technology

Wastewater

FEATURES

Impeller: Cast iron, semi-open or enclosed, nonclog, dynamically balanced with pump out vanes for mechanical seal protection. Optional silicon bronze impeller available.

Casing: Cast iron flanged volute type for maximum efficiency. Designed for easy installation on A10-20 guide rail.

Dual Mechanical Seals

- Lower: SILICON CARBIDE VS. SILICON CARBIDE sealing faces for superior abrasive resistance, stainless steel metal parts, BUNA-N elastomers.
- Upper: CARBON VS. CERAMIC sealing faces, stainless steel metal parts, BUNA-N elastomers.

Seal Sensor Probe: Located in oil-filled chamber. If pumpage should begin to leak past lower seal it indicates to pump control panel a fault has occurred. Requires optional Seal Fail Circuit in the control panel.

APPLICATIONS

Specifically designed for the following uses:

- Sewage systems
- Dewatering/Effluent
- Water transfer
- Light industrial
- Commercial applications

Anywhere waste or drainage must be disposed of quickly, quietly and efficiently.

SPECIFICATIONS

Pump:

- Solids handling capabilities: 2" maximum.
- Capacities: up to 183 GPM.
- Total heads: up to 52' TDH.
- Discharge size: 2" NPT threaded companion flange on 2WD. 3" NPT threaded companion flange on 3WD.
- Temperature: 104° F (40° C) continuous, 140° F (60° C) intermittent.

MOTORS

- Fully submerged in high grade turbine oil for lubrication and efficient heat transfer. All ratings are within the working limits of the motor.
- Class F insulation

Shaft: Corrosion resistant, 400 stainless steel. Threaded design. Locknut on all models to guard against component damage on accidental reverse rotation.

Fasteners: 300 series stainless steel.

Capable of running dry without damage to components.

Designed for continuous operation when fully submerged.

AGENCY LISTINGS



Tested to UL 778 and CSA 22.2 108 Standards
 By Canadian Standards Association
 File #LR38549

Single phase (60 Hz):

- All single phase models feature capacitor start motors for maximum starting torque.
- Built-in overload with automatic reset.
- ½ and ½ HP 16/3 SJTOW with 115 V or 230 V three prong plug.
- $\frac{3}{4}$ and 1 HP 14/3 STOW with bare leads.

Three phase (60 Hz):

- Overload protection must be provided in starter unit.
- $\frac{1}{2}$ -1 HP 14/4 STOW with bare leads.
- Designed for Continuous Operation: Pump ratings are within the motor manufacturer's recommended working limits, can be operated continuously without damage when fully submerged.
- Bearings: Upper and lower heavy duty ball bearing construction.
- Power and Control Cable: Severe duty rated, oil and water resistant. Epoxy seal on motor end provides secondary moisture barrier in case of outer jacket damage and to prevent oil wicking. 20 foot standard with optional lengths available.

Goulds Water Technology

MODEL AND MOTOR INFORMATION

Order		DL	Value	DDM	Impe	ller	Maximum	L.R.	KVA	F.L. Motor	Resi	stance	Wt.					
Number	HP	Phase	Volts	RPM	Dia. (in.)	Code	Amps	Amps	Code	Efficiency %	Start	Line-Line	(lbs.)					
2WD52B0EA			115				10.7	30.0	М	54	11.9	1.7						
2WD52B8EA	0.33	1	208		4.69	E	6.8	19.5	к	51	9.1	4.2	90					
2WD52B1EA]		230				4.9	14.1	L	53	14.5	8.0						
2WD52C0DA			115				14.5	31.1	J	55	9.3	1.4						
2WD52C8DA	1	1	208			D	8.0	19.5	к	51	9.1	4.2	94					
2WD52C1DA	1		230				7.3	16.5	J	54	11.7	5.6						
2WD52C2DA	0.5		200		5.00		3.8	12.3	К	75	NA	6.7						
2WD52C3DA	1		230				3.3	9.7	к	75	NA	9.9						
2WD52C4DA	1	3	460				1.7	4.9	к	75	NA	39.4						
2WD52C5DA	1		575				1.4	4.3	к	68	NA	47.8						
2WD52D8CA			208				11.0	39.0	к	65	2.6	1.4						
2WD52D1CA		1	230	1750			9.4	24.8	J	57	4.8	2.3						
2WD52D2CA			200				4.1	21.2	н	74	NA	4.3						
2WD52D3CA	0.75		230		5.38	С	3.6	17.3	J	76	NA	5.6	98					
2WD52D4CA		3	460				1.8	8.9	J	76	NA	22.4						
2WD52D5CA			575	-			1.5	7.3	J	71	NA	29.2						
2WD52E8BA			208				14.0	39.0	к	65	2.6	1.4						
2WD52E1BA	-	1	230				12.3	30.5	н	60	4.3	1.8						
2WD52E2BA			200			6.0	21.2	н	74	NA	4.3							
2WD52E3BA	1		230		5.75	В	5.8	17.3	J	76	NA	5.6	104					
2WD52E4BA		3	460				2.9	8.9	J	76	NA	22.4						
2WD52E5BA			575				2.4	7.3	J	71	NA	29.2						
2WD51B0KA			115				12.4	46.0	M	54	7.5	1.0						
2WD51B8KA	0.33	1	208		2.94	К	6.8	31.0	K	68	9.7	2.4	90					
2WD51B1KA			230	-	2.77	K	6.2	34.5	M	53	9.6	4.0						
2WD51C0JA			115				14.5	46.0	M	54	7.5	1.0						
2WD51C8JA	-	1	208				8.4	31.0	К	68	9.7	2.4						
2WD51C1JA	-		230				7.6	34.5	M	53	9.6	4.0						
2WD51C2JA	0.5	0.5	0.5	0.5	0.5	0.5		200	-	3.19		4.9	22.6	R	68	NA	3.8	94
2WD51C3JA							0.0	0.0						230		0.17	J	3.6
2WD51C4JA	-	3	460				1.8	9.4	R	70	NA	23.2						
2WD51C5JA	-		575				1.5	7.5	R	62	NA	35.3						
2WD51D8HA			208				11.0	31.0	к	68	9.7	2.4						
2WD51D1HA	-	1	230	3500			10.0	27.5	J	65	12.2	2.7						
2WD51D2HA			200				6.2	20.6	L	64	NA	5.7						
2WD51D3HA	0.75		230		3.44	Н	5.4	15.7	К	68	NA	8.6	98					
2WD51D4HA		3 460		2.7	7.9	К	68	NA	34.2									
2WD51D5HA			575				2.2	9.9	L	78	NA	26.5						
2WD51E8AA			208				14.5	59.0	К	68	9.3	1.1						
2WD51E1AA		1	200				13.0	36.2	J	69	10.3	2.1						
2WD51E1AA 2WD51E2AA			230				8.6	37.6	M	77	NA	2.1						
2WD51E3AA	1		230		3.75	А	7.5	24.1	L	79		4.1	104					
		3								79	NA							
2WD51E4AA			460 575				3.8	12.1 9.9	L		NA	16.2						
2WD51E5AA					the 1st chara		3.1	7.7	L	78	NA	26.5						

To order a pump with a 3" NPT discharge, change the 1st character to a 3, ex. 3WD51E5AA

APPLICATION DATA

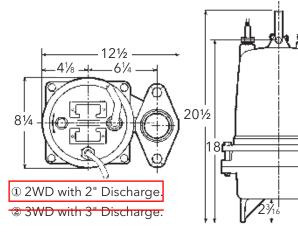
Maximum Solid Size	2"			
Minimum Casing Thickness	5%6"			
Casing Corrosion Allowance	1/8"			
Maximum Working Pressure	22 PSI			
Maximum Submergence	50 feet			
Minimum Culomenance	Fully submerged for continuous operation			
Minimum Submergence	6" below top of motor for intermittent operation			
Maximum Environmental Temperature	40°C (104°F) continuous operation			
waximum Environmental temperature	60°C (140°F) intermittent operation			

CONSTRUCTION DETAILS

	16/3, type SJTOW: single phase, ½ HP			
Power Cable - Type	14/3, type STOW: single phase, ¾ & 1 HP			
	14/4, type STOW: all three phase			
Sensor Cable - Type	16/2, type SJTOW: seal sensor only			
Selisor Cable - Type	18/4, type SJTOW: optional seal/heat sensor			
Motor Cover	Gray Cast Iron - ASTM A48 Class 30			
Bearing Housing	Gray Cast Iron - ASTM A48 Class 30			
Seal Housing	Gray Cast Iron - ASTM A48 Class 30			
Casing	Gray Cast Iron - ASTM A48 Class 30			
Impeller	Gray Cast Iron - ASTM A48 or Cast Bronze - ASTM B584 C87600			
Motor Shaft	AISI 300 Series Stainless Steel			
Motor Design	NEMA 48 Frame, oil filled with Class F Insulation			
Materia Constant Destanting	Single Phase: on winding thermal overload protection			
Motor Overload Protection	Three Phase: require ambient compensated Class 10, quick trip overloads in the control panel.			
Motor Seal Fail (Moisture) Detection	Seal fail sensor in an oil-filled seal chamber. Connect to an optional relay in control panel.			
Optional Motor Thermal Protection	Normally closed on-winding thermostats open at 275° F (135 °C) and close at 112° F (78° C). Require terminal connection in the control panel.			
External Hardware	300 Series Stainless Steel			
	Semi-opened with pump out vanes on back shroud - 1750 RPM			
Impeller Type	Enclosed with pump out vanes on back shroud - 3500 RPM			
Oil Capacity - Seal Chamber	10 ounces			
Oil Capacity - Motor Chamber	4.0 quarts			

STANDARD PARTS

Dell Deerier	Upper	Single row ball - SKF™ 6203-2Z		
Ball Bearing	Lower	Single row ball - SKF™ 6203-2Z		
Mechanical Seals - Standard	Upper	Carbon/Ceramic; John Crane Type 6		
Mechanical Seals - Standard	Lower	Silicon Carbon/Silicon Carbon; Type 16		
Mechanical Seals - Optional Lower		Silicon Carbide/Tungsten Carbide: Type 16		
O-Ring – Stuffing Box		BUNA-N, AS 568A-163		
O-Ring - Motor Cover		BUNA-N, AS 568A-166		



DIMENSIONS

3" NPT- 2" NPT-

71/8

61/8

12

(All dimensions are in inches. Do not use for construction purposes.)

NOMENCLATURE DESCRIPTION

1st Character - Discharge Size

2 = 2" discharge 3 = 3" discharge

2nd and 3rd Characters - Series/Solids Size

WD = wastewater, 2" solids handling, dual seal with seal fail probe in pump.

4th Character - Mechanical Seals

- 5 = silicon carbide/silicon carbide/BUNA lower seal and carbon/ceramic/BUNA - upper seal (standard)
- 3 = silicon carbide/tungsten carbide/BUNA lower seal and carbon/ceramic/BUNA - upper seal (optional)

5th Character - Cycle/RPM

1 = 60 Hz/3500 RPM	5 = 50 Hz/2900 RPM
2 = 60 Hz/1750 RPM	6 = 50 Hz/1450 RPM

6th Character - Horsepower

B = ⅓ HP	D = ¾ HP
C = ½ HP	E = 1 HP

7th Character - Phase/Voltage/Enclosure

0 = single phase, 115 V	4 = three phase, 460 V
1 = single phase, 230 V	5 = three phase, 575 V
2 = three phase, 200 V	8 = single phase, 208 V
3 = three phase, 230 V	9 = single phase, 220 V, 50 Hz

8th Character - Impeller Diameter

A = 3.75" 1 HP 3500 RPM	E = 4.69" ¹ / ₃ HP 1750 RPM
B = 5.75" 1 HP 1750 RPM	H = 3.44" ³ ⁄ ₄ HP 3500 RPM
C = 5.38" ³ ⁄ ₄ HP 1750 RPM	J = 3.19" 1/2 HP 3500 RPM
D = 5.00" ½ HP 1750 RPM	K = 2.94" ¹ / ₃ HP 3500 RPM

9th Character - Cord Length (Power and Sensor)

A = 20' (standard)	F = 50'
D = 30'	J = 100'

10th Character - Options

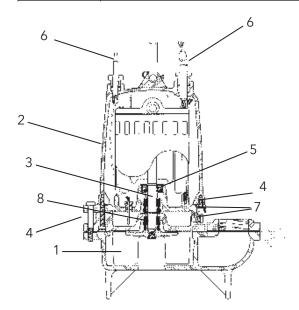
B = Bronze impeller	E = Epoxy paint
F = Both epoxy paint	and bronze impeller

Last Character - Option

H = Pilot duty thermal sensors (3 phase only!!)

MATERIALS OF CONSTRUCTION

ltem	Dent				Ν	late	rial	
No.	Part Name				Standard	0	ptional	
1	Impeller				1003			1179
2	Motor cover				1003			
3	Shaft				300 Series	SS		
4	Fasten	ers			300 Series	SS		
5	Ball bearings				Steel			
6 -	Power	cable		STOW, 20 fee		ot	Additional lengths	
0	Seal se	ensor cabl	е			eet		
7	O-ring			BUNA-N				
	Outer Mech. Seal	Service	Rotary		Stationary	Elasto- mers		Metal Parts
8	OPT	Heavy duty	Silicon Carbide		Tungsten Carbide	BUNA-N		300 Series SS
	STD	Mild abrasives	Silico	on Carbide		BUNA-N		300 Series SS
	Mater		Engineering Standard				1	
	1	Cast iron – ASTM A48 Class 30				is 30		
	1	1179			Silicon bronze – ASTM C87600			



Goulds Water Technology

STANDARD PANEL OPTIONS

mp Order Number	Boulay	y Series	Disconnect Style			
•	Simplex	Duplex	Simplex	Duplex		
2WD52B0EA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD52B8EA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD52B1EA	S10020H	D10020J	CSD14063H	CDD14063J		
2WD52C0DA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD52C8DA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD52C1DA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD52C2DA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD52C3DA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD52C4DA	S31615H	D31615J	CSD31625H	CDD31625J		
2WD52C5DA	S31615H	D31615J	CSD31625H	CDD31625J		
2WD52D8CA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD52D1CA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD52D2CA	S34063H	D34063J	CSD14063H	CDD14063J		
2WD52D3CA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD52D4CA	S31625H	D31625J	CSD31625H	CDD31625J		
2WD52D5CA	S31625H	D31625J	CSD31625H	CDD31625J		
2WD52E8BA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD52E1BA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD52E2BA	S34063H	D34063J	CSD34063H	CDD34063J		
2WD52E3BA	S34063H	D34063J	CSD34063H	CDD34063J		
2WD52E4BA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD52E5BA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD51B0KA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD51B8KA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD51B1KA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD51C0JA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD51C8JA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD51C1JA	S10020H	D10020J	CSD16310H	CDD16310J		
2WD51C2JA	S34063H	D34063J	CSD34063H	CDD34063J		
2WD51C3JA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD51C4JA	S31625H	D31625J	CSD31625H	CDD31625J		
2WD51C5JA	S31625H	D31625J	CSD31625H	CDD31625J		
2WD51D8HA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD51D1HA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD51D2HA	S34063H	D34063J	CSD34063H	CDD34063J		
2WD51D3HA	S34063H	D34063J	CSD34063H	CDD34063J		
2WD51D4HA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD51D5HA	S31625H	D31625J	CSD31625H	CDD31625J		
2WD51E8AA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD51E1AA	S10020H	D10020J	CSD11016H	CDD11016J		
2WD51E2AA	S36310H	D36310J	CSD36310H	CDD36310J		
2WD51E3AA	S36310H	D36310J	CSD36310H	CDD36310J		
2WD51E4AA	S32540H	D32540J	CSD32540H	CDD32540J		
2WD51E5AA	S32540H	D32540J	CSD32540H	CDD32540J		

Note: Panel part numbers above do not include float switches

Note: Panel part numbers above include a seal fail circuit. If the 3 phase high temperature option is chosen for the pumps (H suffix), add an M suffix to the simplex part numbers above or an N suffix to the duplex models

Note: All panel part numbers above have additional available features, see page 7 for more information.

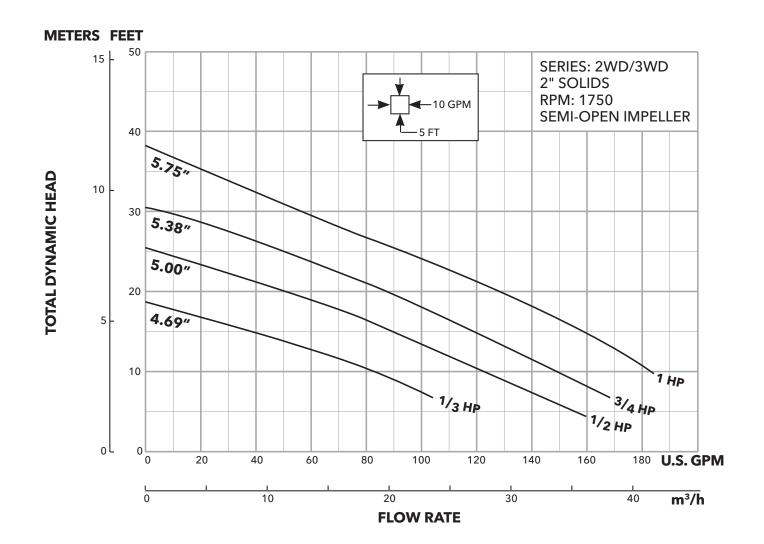


PERFORMANCE CURVES

C2WD/3WD

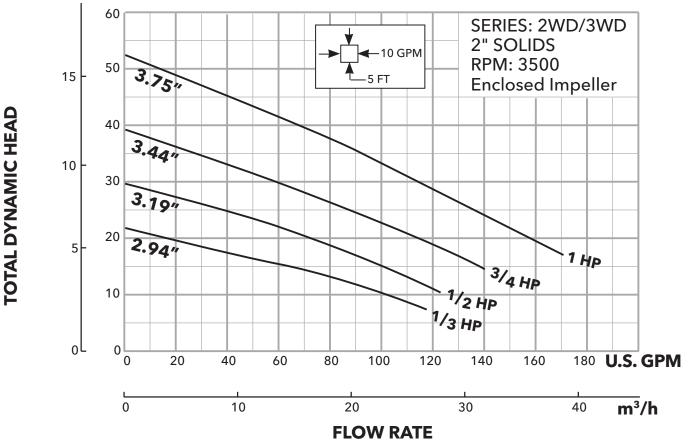
2WD/3WD Submersible 2" Non-Clog Sewage Pump

Impeller Diameter	Impeller Code	Motor HP Rating
5.75"	В	1
5.38"	С	3⁄4
5.00"	D	1/2
4.69"	E	1/3



Impeller Diameter	Impeller Code	Motor HP Rating
3.75"	А	1
3.44"	Н	3⁄4
3.19"	J	1/2
2.94"	К	1/3





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Goulds Water Technology

Wastewater





BOULAY SERIES

- NEMA 4X outdoor rated enclosure
- Red alarm beacon
- HOA selector switch
- Through door pump run light(s)
- Through door alarm test and horn silence button
- Single phase models handle 120, 208 and 230V service
- Three phase models handle 200, 230, 460 and 575V service
- Accepts single or dual power feed
- See brochure "BCP3 R11" for additional information on simplex models
- See brochure "BCP4 R14" for additional information on duplex models information

DISCONNECT STYLE

- NEMA 4X outdoor rated enclosure, NEMA 1 also available
- Red alarm beacon
- Through door HOA selector switch
- Through door control on/off switch
- Through door main disconnect switch
- Single phase models handle 120, 208 and 230V service
- Three phase models handle 200, 230, 460 and 575V service
- Accepts single or dual power feed
- See brochure "BCPSDWWP R3" for additional information

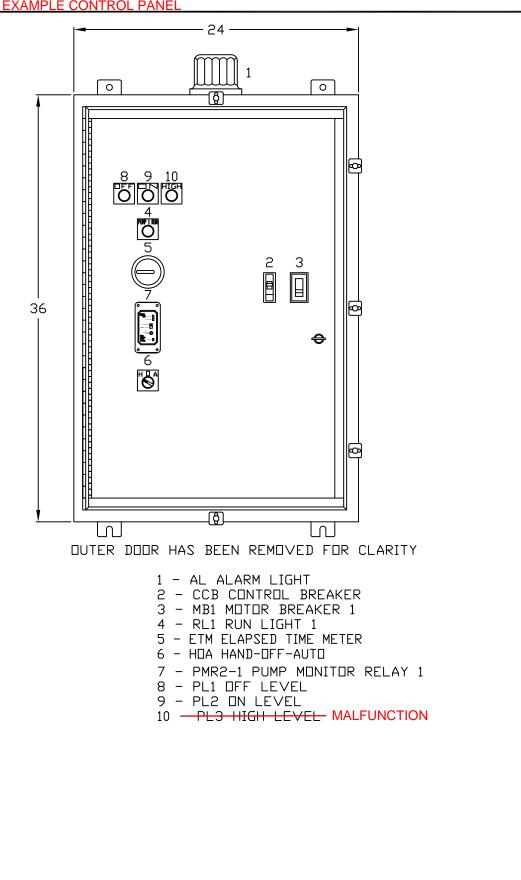
CONTRACTOR SHALL COORDINATE WITH MANUFACTURER TO ACQUIRE COMPATIBLE PUMP AND CONTROL PANEL. ADDITIONALLY, THE CONTRACTOR WILL COORDINATE WITH THE MANUFACTURER TO PROGRAM THE PUMP TO THE FOLLOWING SPECIFICATIONS:

- THE PROPOSED PUMP SHALL ONLY FUNCTION ABOVE ELEVATION 6.20.
- PUMP SHALL ONLY BEGINNING "ON" FUNCTIONS WHEN THE WATER ELEVATION IS ABOVE ELEVATION OF 6.20.

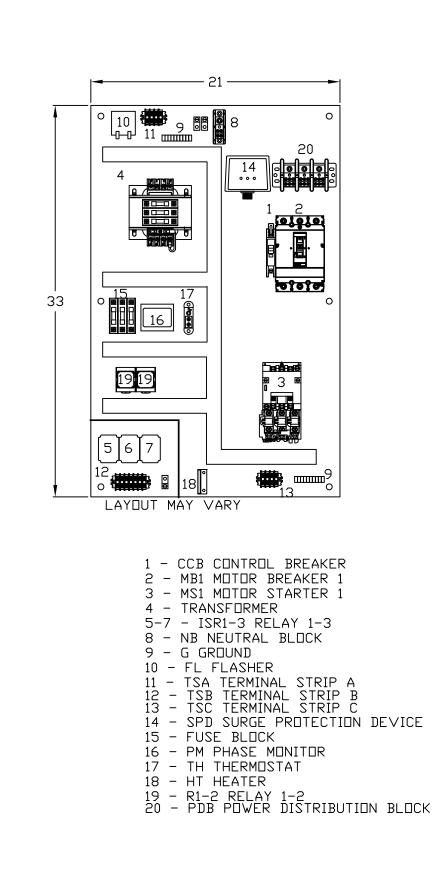
CONTRACTOR SHALL CONSTRUCT THE STRUCTURE AND DEVICE TO ENSURE THAT THE FLOAT SWITCHES WILL RECOGNIZE THE CORRECT ELEVATIONS IN ORDER FOR THE WATER LEVEL TO ALWAYS COVER THE PUMP IMPELLER DURING "ON" FUNCTIONS.

THE CONTROL PANEL FOR THE PUMP SHALL ALSO BE PROGRAMMED TO ALERT THE OWNER WHEN THE PUMP IS ACTIVE AND RUNNING NORMALLY OR WHEN PUMP IS TRIGGERED ON BUT NO MOVEMENT IS RECOGNIZED OR MALFUNCTION HAS OCCURRED.

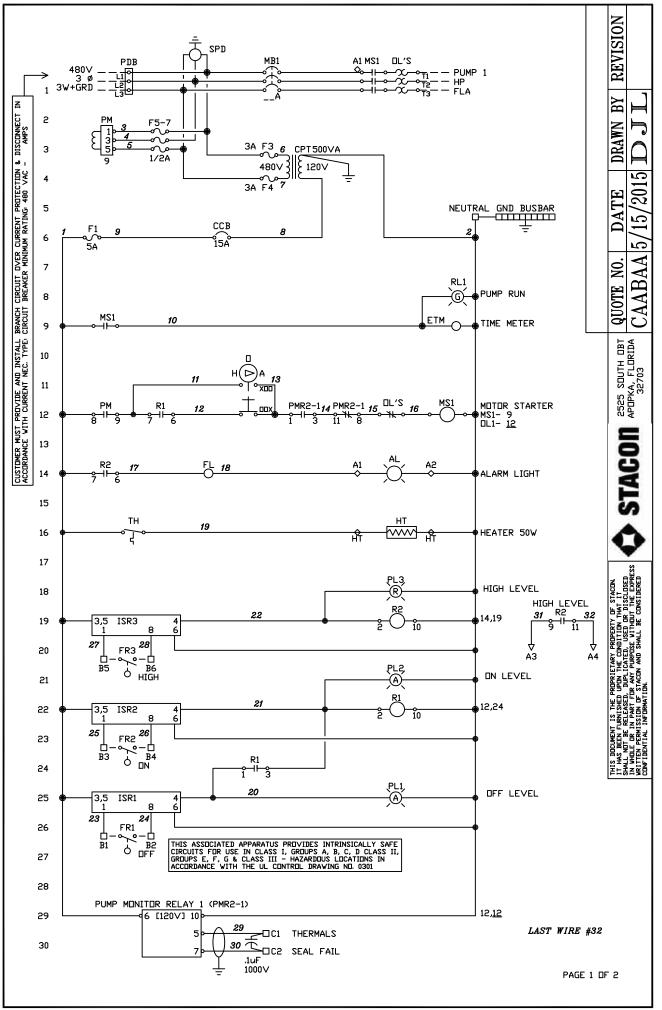
EXAMPLE CONTROL PANEL

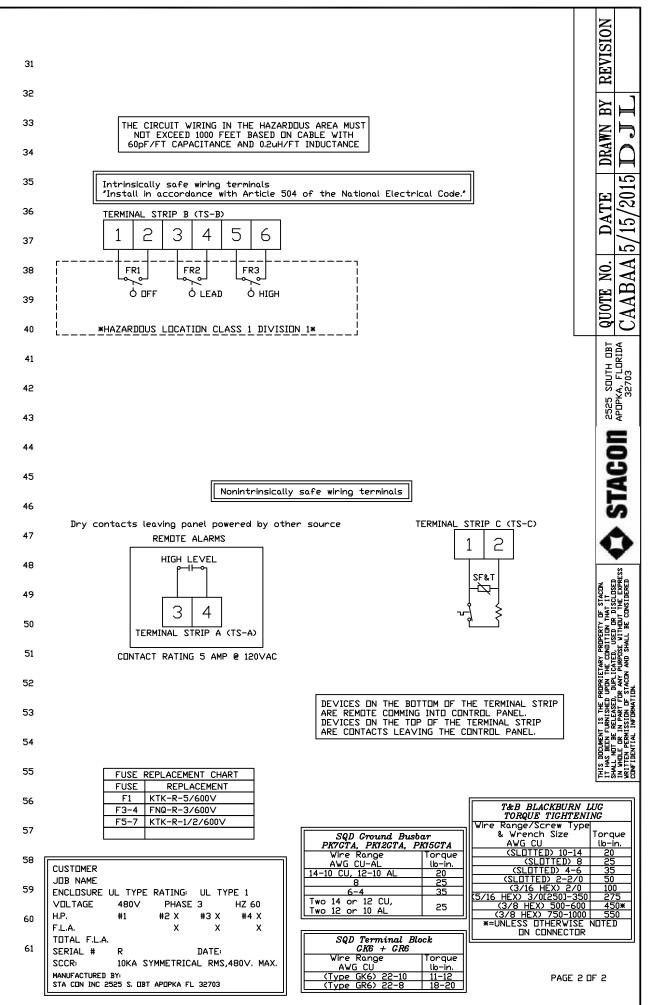












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PHASE 2: 1320 WILLOW ROAD Preliminary Hydrology Report

February 3, 2023

C20181310

PREPARED FOR: **DES Architects + Engineers, Inc.** 399 Bradford St. Redwood City, CA

> On behalf of **Tarlton Properties, Inc.** 1530 O'Brien Dr., Suite C Menlo Park, CA



PREPARED BY OR UNDER DIRECTION OF: BKF ENGINEERS 150 California St, Suite 600 San Francisco, CA 94111 Mike O'Connell P.E. CA 75811

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Figure 8: FEMA Insurance Rate Map

APPENDICES

Appendix A: Menlo Park Hydrology Requirements – Attachments A and B Appendix B: City of Menlo Park Impervious Area Worksheet Appendix C: Existing Conditions Topographic Survey

1. INTRODUCTION

Tarlton Properties, Inc. (Tarlton Properties), has proposed a redevelopment of three parcels in Menlo Park currently containing three buildings: 985 and 1001/1015 O'Brien Drive and 1320 Willow Road. The existing buildings are planned to be replaced with two new buildings to be identified as 1005 O'Brien Drive and 1320 Willow Road, and a parking garage, along with other various site improvements. The overall project is split into two phases. This report will only consider the improvements and redevelopment occurring within Phase 2, unless otherwise stated.

The purpose of this report is to document the existing drainage conditions in and around the subject property as well as the design of the proposed storm water conveyance and management facilities per the City of Menlo Park Drainage Guidelines (City Guidelines). All elevations presented in this report are on the NAVD 88 datum.

2. OVERVIEW

With regards to the overall project scope, Tarlton Properties intends to redevelop the three parcels currently containing 985 and 1001/1015 O'Brien Drive and 1320 Willow Road. The site location can be seen in Figure 1 below. The existing buildings are planned to be demolished and replaced with new structures, identified as 1005 O'Brien Drive, 1320 Willow Road, as well as a new multi-level parking garage. This is to be segmented into two phases: Phase 1 includes developing 1005 O'Brien Drive and the parking garage, Phase 2 includes constructing a new 1320 Willow Road building. Both phases will include utility work and other various site enhancements, including stormwater treatment.

The Phase 2 project site is approximately 0.85 acres and is bound to the north by a parking lot and playing field adjacent to Mid-Peninsula High School and the San Francisco Public Utility Commission (SFPUC) / Hetch Hetchy parcel. Willow Road borders the site to the west. To the south, Phase 2 is bordered by 965 and 935 O'Brien Drive and a Menlo Park sanitary sewer lift station. At the time that Phase 2 is ready to commence, the Phase 1 improvements will have been completed and will also border the property to the south and east.

Phase 1 will be constructed to the south and east of Phase 2 and includes a partial demolition of the eastern portion of 1320 Willow Road coupled with the installation of an interim exterior wall. The properties to the south, 965 and 935 O'Brien Drive, as well as the sanitary sewer lift station, will all remain undisturbed through Phases 1 and 2.

The overall existing site is composed of industrial businesses encompassing a gross floor area of approximately 90,630 square feet, parking areas, and minor landscape features. In the existing condition, the Phase 2 area is approximately 93% covered with impervious surface. Phase 2 intends to significantly increase the site's pervious area by adding approximately 6,264 square feet of new pervious surface. This will subsequently lower the impervious area to approximately 76%. The modified landscape area will include two bioretention basins to treat run-off from the site.



Preliminary Hydrology Report February 3, 2023

The project site is located near the downstream end of the drainage shed noted as the San Francisco Bay drainage basin; based on Attachment A of the City of Menlo Park Requirements for the Preparation of Hydrology Reports (City Hydrology Requirements). The site is outside of the problem areas indicated in Attachment B of the City Hydrology Requirements, thus not requiring hydrograph modifications. Both attachments are included in Appendix A of this report. The site is not connected to any of the storm drainage systems analyzed as a part of the May 2003 City-wide Drainage Study. Therefore, it is assumed the system that this site's storm drain will discharge to has no capacity issues.

The current Federal Emergency Management Agency (FEMA) base flood elevation (BFE) for the site was determined to be between elevations 11 to 13 based on the Federal Emergency Management Agency Insurance Rate Map (FIRM) dated April 5, 2019. The flood elevation was determined by DES Engineers to be 12.8. The site is located within Zone AE which is indicated as a Special Flood Hazard Area. Coastal transect boundary and intersection B49, which approximately delineates the coastal flood zones, is located within the SFPUC parcel directly north of the project. The currently available FEMA Insurance Rate Map is attached as Figure 8. The proposed finished grades for the project range between elevations 11.50 at the lowest connection to the existing condition and 14.80 as the finished floor of both the proposed building and garage. Therefore, the finished floors of the buildings and the garage will be 2 feet above the determined BFE. Note that the BFE is the flood elevation that will occur during a 100-year storm event.



Figure 1: Vicinity Map



3. EXISTING DRAINAGE CONDITION

The regional drainage pattern in the vicinity of the project site appears to be from south to north. The project site itself does not have a known underground storm drain system but instead relies on overland flow to direct the majority of the storm water run-off to a valley gutter internal to the property. The on-site storm water is primarily collected via the valley gutter and drained from the east to west, toward the Willow Road driveway. Run-off then drains from the valley gutter to the curb flowline along Willow Road. Stormwater flows along the flowline until it is collected by a catch basin north of the property. The catch basin is directly connected to a 66-inch storm drain main in Willow Road. The existing conditions for the site and immediate area can be seen in the attached Figure 3 and Appendix C.

3.1 ON-SITE DRAINAGE

As stated, the site does not have a known underground storm drain system. A survey performed by Kier+Wright indicates one on-site catch basin at the bottom of a subgrade truck ramp with no recorded outlets. The survey did not indicate any pump facilities or other potential outlets for the catch basin around the perimeter of the site, nor other structures for it to connect to. Therefore, it is assumed that run-off from the existing roof water leaders is discharged directly to the hardscape surface where it, and the other storm water, collect in the on-site valley gutter for overland release. The site relies almost completely on overland flow to discharge storm water from the property to Except for the stormwater draining down the dock ramp, which held in the single on-site catch basin, the site relies almost completely on overland flow to discharge storm water. Currently, there are no known storm water management facilities on-site that provide significant treatment or detention.

3.2 OFF-SITE DRAINAGE

Off-site drainage immediately around the project site is limited to overland flow along Willow Road and overland flow onto and through the SFPUC's parcel. Phase 2 does not drain to the SFPUC parcel, but instead outfalls to Willow Road. Willow Road along Phase 2's frontage has a vertical curb, most of which is not accompanied by a gutter pan. Nevertheless, stormwater is directed north along the curb flowline to a catch basin in the City's right of way, just north of the project. GIS files provided by the City of Menlo Park show the catch basin is connected to the 66-inch storm drain main in Willow Road. The large storm drain main eventually discharges to a pump station adjacent to Bayfront Expressway where it is then transferred to a slough connected to the San Francisco Bay.

The adjacent Phase 1 parcel currently drains to the SFPUC parcel and is picked up by the existing 48-inch storm drain main east of the project site. Flow through the 48-inch storm drain line is part of a separate system and does not appear to receive tributary flow from the Phase 2 site. Both the 48 and 66 -inch lines ultimately discharge to the San Francisco Bay.

The drainage area for the 66-inch line appears to lie almost exclusively within Menlo Park's jurisdiction. Off-site drainage to the 66-inch line was approximately delineated only for the purpose of visualizing a reasonable tributary area. It is not intended to provide a detailed analysis of off-site system and drainage pattern. Refer to the attached Figure 2 for the off-site drainage area delineation map.



4. BASIS OF DESIGN

The following summarizes the basis of design for the corresponding calculations found in the attached Tables 2 and 3.

Determination of site design flow rates are based on the Rational Method: The Rational Method is defined as Q = C I A, where:

- Q = peak flow (cfs)
- C = run-off coefficient
- I = rainfall intensity (in/hr)
- A = area (acres)

Design Storm Event: The storm drain system is evaluated for a 10-year storm event.

Time of Concentration: For this report, on-site time of concentration is assumed to be 10 minutes.

Run-off Coefficient: Run-off coefficients are developed using the City of Menlo Park Requirements for the Preparation of Hydrology Reports (August 20, 2006). Run-off coefficient of 0.95 was used for all impervious areas. Run-off coefficient of 0.3 was used for all pervious and landscaped areas based on the upper limit of the Coefficient of Run-off chart provided within the City Hydrology Requirements. A weighted run-off coefficient of 0.904 and 0.795 were calculated and implemented for the existing and proposed coefficients, respectively.

Rainfall Intensity: The rainfall intensity for the 10-year design storm event was calculated using Attachment C - Menlo Park IDF Curve.

Freeboard: The existing system is evaluated against the 10-year event contained within the storm drain system.

Rim Elevations: Rim elevations are based on a combination of the DES Architects+ Engineers (DES) grading plan and the topographic survey for the site.



5. PROJECT IMPROVEMENTS

Tarlton Properties intends to completely demolish the western portion of 1320 Willow Road. The eastern portion of the building is planned to be demolished and the building will be closed off with a new exterior wall as an interim condition in Phase 1. After demolition of the building and surrounding site, a new office building, landscaping and supporting utilities will be constructed.

With the proposed improvements, Phase 2 is anticipated to add 6,264 square feet of new pervious surface. Subsequently lowering the impervious coverage from 93% to 76%. The project will also be replacing 28,324 square feet of impervious surface. The site proposes to meet storm water treatment requirements by directing run-off to vegetated areas, minimize impervious surfaces, and provide two biotreatment basins.

Storm water will be collected via overland flow which will direct it to a network of new storm drain lines accessed by multiple catch basins throughout the property. Storm water from the new building roof will be directed to the new underground system, through rain water leaders. The new system will convey the flow to the treatment basins on the west side of the property. After filtration in the basins, storm water will exit the property near the northwest corner. The stormwater discharge will gravity flow to the existing 66-inch main in Willow Road via a new connection to an existing manhole.

The proposed invert connection to the public manhole is 7.20. The invert out from the structure is 2.81. This results in 4.39 feet of freeboard between the inverts. If the hydraulic grade line in the 66-inch main rises above the rim elevation of the public manhole, the discharge pipe from the site will be equipped with a check valve. Although the rim elevations of the directly connected structures on-site are higher than the rim elevation of the public manhole, a check valve will further deter stormwater from backflowing onto the property in the event that Menlo Park receives excessive stormwater. The design of the proposed drainage system is depicted in Figure 4: Preliminary Phase 2 Grading Plan and Figure 7: Preliminary Phase 2 Utility Plan.

Noted in Figure 5: Preliminary Phase 2 Stormwater Management Plan, the bioretention areas, PH2-TM#3 & 4, will be located on the west side of the lot. Storm water will be collected from across the site and enter the treatment areas via bubble-up structures at the edges of the basins. A portion of the Phase 2 storm water collected by the roof and ground will be directed to the storm system constructed in Phase 1 and treated by basin PH1-TM#2. All four basins in Phase 1 and 2 are sized larger than required.

PH2-TM#4's two bubble up structures outlet at elevation of 12.30. Likewise, PH2-TM#3's bubble up structure outlets at an elevation of 11.30. Stormwater will either percolate through the treatment soil or collect in the basin until the ponding is 0.25 below PH2-TM#3's and 0.05 feet below PH2-TM#4's bubble up invert. If the storm water level exceeds these ponding elevations, it will flow into overflow structures, bypassing the media filtration. The full design can be seen in Figure 7: Preliminary Phase 2 Utility Plan.

The proposed stormwater drainage design closely mimics the existing drainage conditions. In lieu of overland flow to a public catch basin, the site's stormwater is now proposed to discharge to the same public main at a structure 200 feet closer to the property, reducing surface flow in the public right of way. In the scenario of a high-flow event that overwhelms the basins, excess stormwater will overland release into the public right of way and overland flow to the same public catch basin it does in the existing condition.



5.1 STORMWATER MANAGEMENT

The project will create or replace approximately 28,324 square feet of impervious area and convert 6,264 square feet of existing impervious surface to pervious surface. See Table 1: Existing vs Proposed Area Summary below for the changes regarding existing and proposed allocations of impervious and pervious areas.

Per the San Mateo Countywide Water Pollution Prevention program (SMCWPPP) C.3 Stormwater Handbook, "Projects that create and/or replace 10,000 square feet or more of impervious surface must comply with Provision C.3". The proposed improvements meet this threshold, and therefore qualify as a Regulated Project and must include treatment measures.

To meet C.3 requirements, the proposed treatment basins are sized based on the Flow and Volume method and calculated per Section 5.1.3 of C.3 Regulated Projects. Four proposed treatment basins between Phases 1 & 2 are intended to capture and treat run-off from the site. Refer to Figures 4 through 7 for an overview of the proposed drainage system and stormwater management plan.

	Area (ft²)				
	Existing Proposed Delta				
Impervious	34,588	28,324	-6,264		
Pervious	2,612	8,876	+6,264		
Total	37,200	37,200	0		

Table 1: Phase 2 Existing vs Proposed Area Summary

It should be noted that the drainage management areas between Phase 1 and Phase 2 overlap. Nevertheless, in its final condition the site will have more treatment than required for the proposed improvements. This is documented in Figure 5: Preliminary Phase 2 Stormwater Management Plan. For reference, Figure 6: Preliminary Overall Stormwater Management Plan depicts the stormwater treatment plan after completion of both Phase 1 and Phase 2.

The Menlo Park Impervious Area Worksheet prepared by DES is provided under Appendix B of this report. The SMCWPPP C.3 checklist will be provided by DES under a separate submittal with the Stormwater Management Plan.



5.2 DETENTION FACILITIES

The City Guidelines require an on-site retention (or detention where retention is impracticable) device if a project increases run-off to the public storm drain system during a 10-year storm event. As shown in Tables 2 and 3, the existing discharge is estimated to be 1.58 cfs and the proposed site discharge is estimated to be 1.39 cfs. These values were calculated using the City Guidelines. The reduction is due to the addition of 6,264 square feet of new pervious area. Therefore, the total amount of discharge to the public storm drain system will be reduced, and the project will not need to implement a retention or detention device. The project will, however, install two biotreatment facilities to conform to C3 guidelines.

6. STORM DRAIN ANALYSES

The proposed system will collect run-off from the site and convey it to PH2-TM#3 & 4. After filtering through the treatment areas, the storm water will exit the Phase 2 side of the site via gravity to an existing off-site manhole. This marginally differs from the existing condition, as it will no longer discharge overland to City curb's flowline. Instead it will discharge directly to a closer structure connected to the same 66-inch public collector main it is currently tributary to.

Preliminary calculations of the system performed by DES, shown in attached Tables 2 and 3, indicate that the existing discharge for a 10-year storm to the off-site system is approximately 1.58 cfs. The proposed discharge for a 10-year storm to the off-site system was calculated to be 1.39 cfs. The proposed discharge is expected to be less than the existing discharge, therefore, no adverse effects to the existing off-site system are anticipated. A proposed check valve on the outfall pipe from Phase 2 will further assist in preventing backflow onto the property in the event the hydraulic grade line rises above the rim elevation of the public manhole.



7. CONCLUSION

The existing project site is served by overland flow to a valley gutter internal to the property. The valley gutter discharges via overland flow to the curb flowline in the City's right of way. Currently there are no known storm water management facilities on-site that provide significant treatment or detention. The discharge of the existing system was estimated to be 1.58 cfs.

The proposed project improvements include replacing the existing building and paved lot on the property with a new office building, bioretention planters, impervious area, and pervious landscaping.

With the proposed improvements, the project is anticipated to add 6,264 square feet of new pervious surface and create or replace approximately 28,324 square feet of impervious surface. As a result of the increase in pervious surface, the proposed discharge will decrease to 1.39 cfs.

To meet C.3 requirements, the project proposes to implement two bioretention basins. The treatment areas are sized via the Flow and Volume method and will be located on the south side of the site. After flowing through the basins, the storm water will discharge by gravity directly to the public storm drain system.

The existing off-site system has no known capacity issues. With the reduction in total discharge from the site to the same system, no adverse effects to the existing system are expected.



8. REFERENCES

California Regional Water Quality Control Board, San Francisco Bay Region, Municipal Regional Stormwater NPDES Permit, November 28, 2011

City of Menlo Park City-wide Drainage Study, May 2003

City of Menlo Park Commercial, Multi-Family and Subdivison Grading & Drainage Guidelines, 2020

City of Menlo Park Impervious Area Worksheet, 2020

City of Menlo Park Requirements for the Preparation of Hydrology Reports, August 20, 2006.

City of Menlo Park Existing Storm Drain GIS, Provided for conceptual reference: January 2023

Federal Emergency Management Agency insurance Rate Map, April 2019

Kier + Wright Topographic Surveys for 1320 Willow Road, 1001-1015 O'Brien Drive, 985 O'Brien Drive, Dated February 2021

Kier + Wright Topographic Surveys for 1340 Willow Road, Dated November 2021

Kier + Wright ALTA / ACSM Land Title Surveys for 1320 Willow Road and 1001-1015 O'Brien Drive, 985 O'Brien Drive, Dated September 2015

Kier + Wright ALTA / ACSM Land Title Surveys for 985 O'Brien Drive, Dated November 2015

San Mateo County C.3 and C.6 Development Review Checklist, January 2019

San Mateo County, C.3 Regulated Projects Guide, Version 1.0., January 2020.



TABLES

TABLE 2 - EXISTING ON-SITE DISCHARGE SUMMARY

PRELIMINARY ON-SITE DISCHARGE CALCULATIONS FOR 1320 Whipple Road (Phase 2)

DES ARCHITECTS+ ENGINEERS

 399 BRADFORD, SUITE 300

 REDWOOD CITY, CA 94063

 Date
 1/6/2023

 P#
 10025.002

 Source:
 "Requirements for the Preparation of Hydrology Reports" by Menlo Park Public Works (August 2006)

 LAND USE:
 Office Bldg, Parking Garage

 RUNOFF "C":
 0.95(Conc/AC/Roof), 0.30(Landscape)

 Rainfall Intensity 10vr
 Per Attachment C - Menlo Park IDF Curve

Rainfall Intensity 10yrPer Attachment C - Menlo Park IDFTime of Concentration:Initial Tc is assumed to be 7 min.

Total Runoff Q for 10-year is calculated using the Rational Formula (Q=CIA)

Existing Onsite Discharge Summary

Existing On-Site Runoff Coefficient Calculation Summary

Type of Surface	Crunoff	Area (ft ²)	Weight
Impervious	0.95	34,588	32,859
Pervious	0.3	2,612	784
	Total	37,200	33,642
Total Existing Site	0.904		

On-Site Discharge Calculation Summary Q=CIA

Area SF	Area acres	Comp. ^{Coef.} C	СА	Total TIME (MIN.)	INTENSITY II0-yr (IN/HR)	DES. Q (CFS)
37,200	0.854	0.904	0.77	7.00	2.04	1.58

TABLE 3 - PROPOSED ON-SITE DISCHARGE SUMMARY

PRELIMINARY ON-SITE DISCHARGE CALCULATIONS FOR 1320 Whipple Road (Phase 2)

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Proposed Onsite Discharge Summary

Existing On-Site Runoff Coefficient Calculation Summary

Type of Surface	Crunoff		Area (ft²)	Weight	
Impervious		0.95	28,324	26,908	
Pervious		0.3	8,876	2,663	
	Total		37,200	29,571	
Total Existing Site Composite Run-off C = 0.795					

On-Site Discharge Calculation Summary Q=CIA

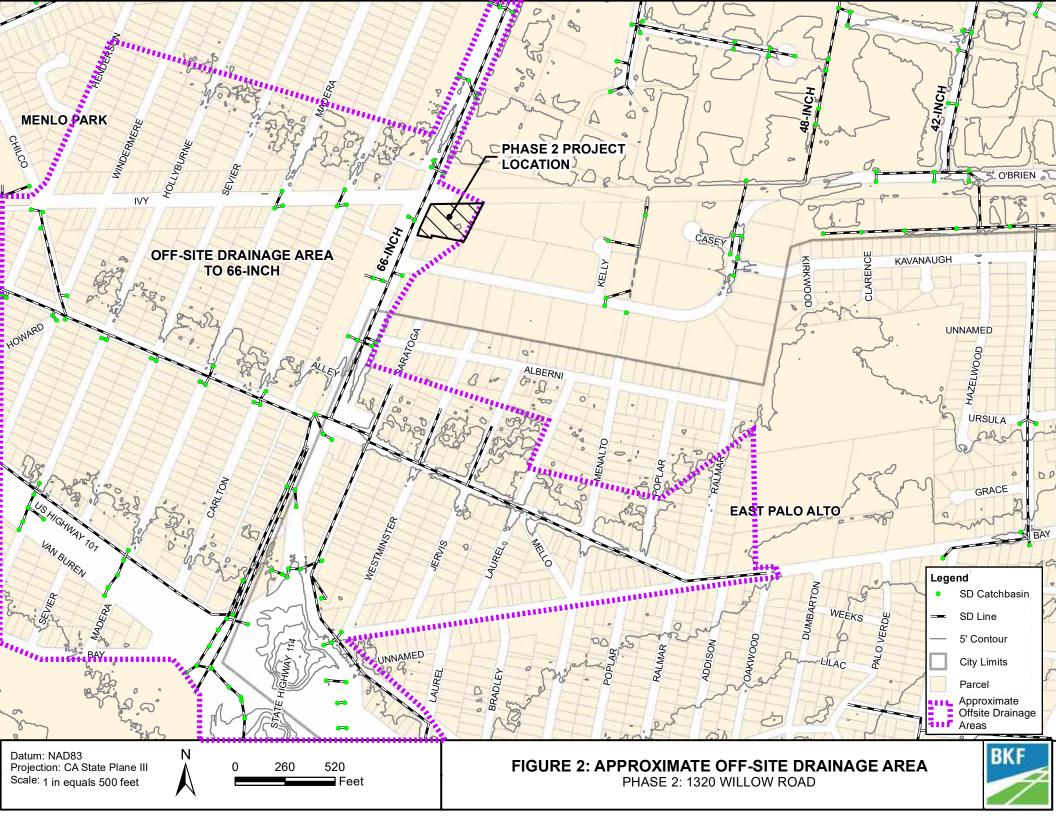
Area SF	Area acres	Comp. ^{Coef.} C	СА	Total TIME (MIN.)	INTENSITY II0-yr (IN/HR)	DES. Q (CFS)
37,200	0.854	0.795	0.68	7.00	2.04	1.39

		w Road Outlet Pipe
Project Description		
Friction Method	Manning	
Solve For	Formula Normal Depth	
	Horman Depart	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.005 ft/ft	
Diameter	12.0 in	
Discharge	1.40 cfs	
Results		
Normal Depth	5.5 in	
Flow Area	0.3 ft ²	
Wetted Perimeter	1.5 ft	
Hydraulic Radius	2.8 in	
Top Width	1.00 ft	
Critical Depth	6.0 in	
Percent Full	45.6 %	
Critical Slope	0.004 ft/ft	
Velocity	4.01 ft/s	
Velocity Head	0.25 ft	
Specific Energy	0.71 ft	
Froude Number	1.194	
Maximum Discharge	3.52 cfs	
Discharge Full	3.27 cfs	
Slope Full	0.001 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	45.6 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	5.5 in	
Critical Depth	6.0 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.004 ft/ft	

1320 Willow Road Outlet Pipe

Untitled1.fm8 10/27/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

FlowMaster [10.03.00.03] Page 1 of 1 FIGURES



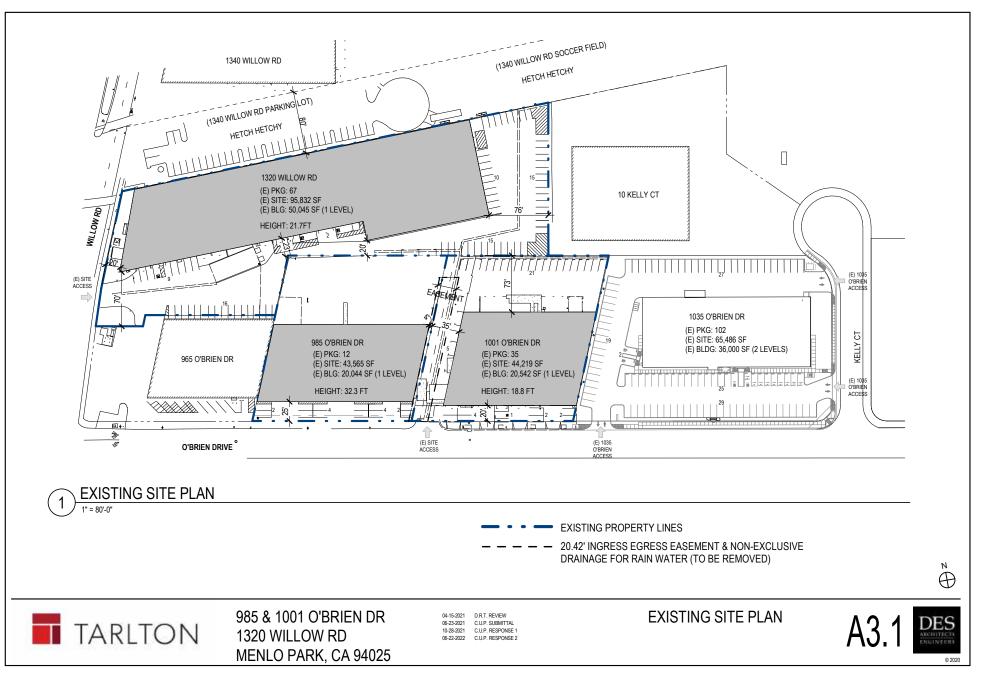


FIGURE 3 - EXISTING CONDITIONS

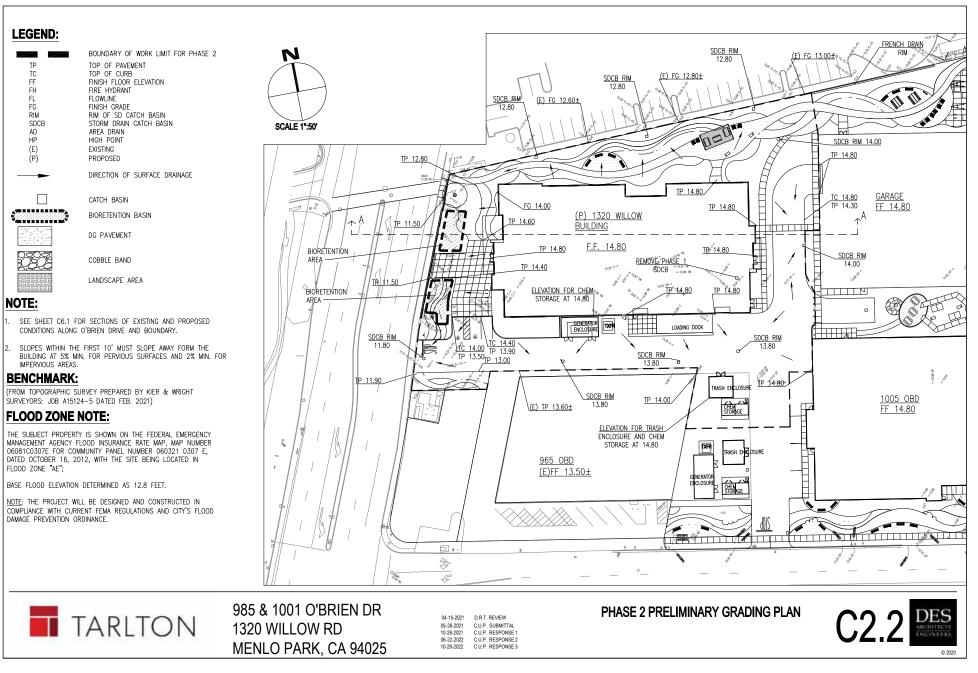
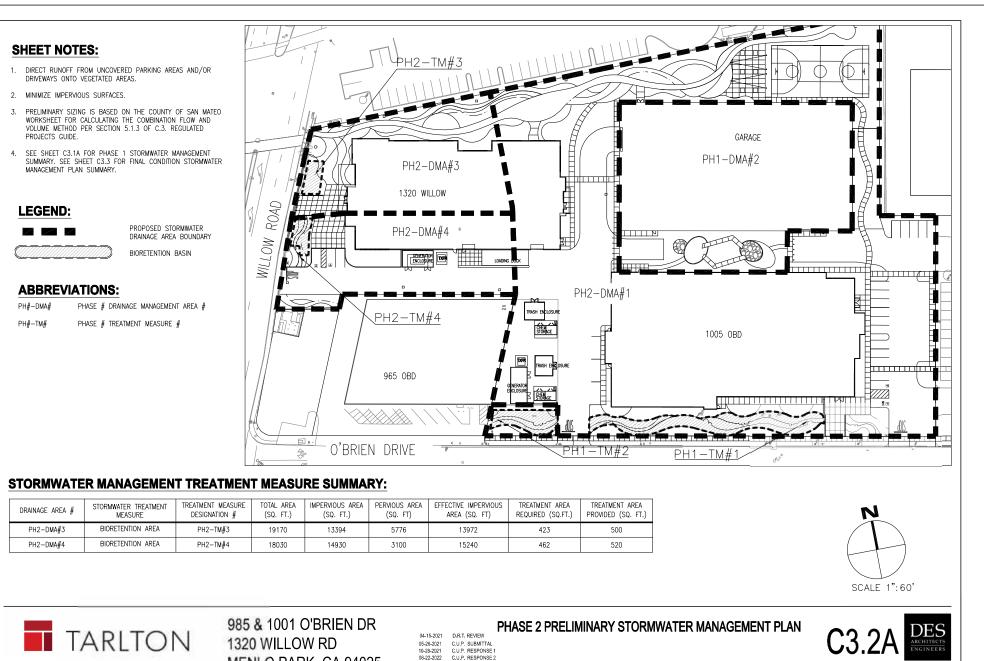


FIGURE 4 - PRELIMINARY PHASE 2 GRADING PLAN DATED 01/06/2023

BIM 360://Tartton - 1005 OBD/1 0025002_A_1005OBD_SHELL_2020_

Central



MENLO PARK, CA 94025

10-28-2022

C.U.P. RESPONSE 3

FIGURE 5 - PRELIMINARY PHASE 2 STORMWATER MANAGEMENT PLAN DATED 02/01/2023

@ 2020

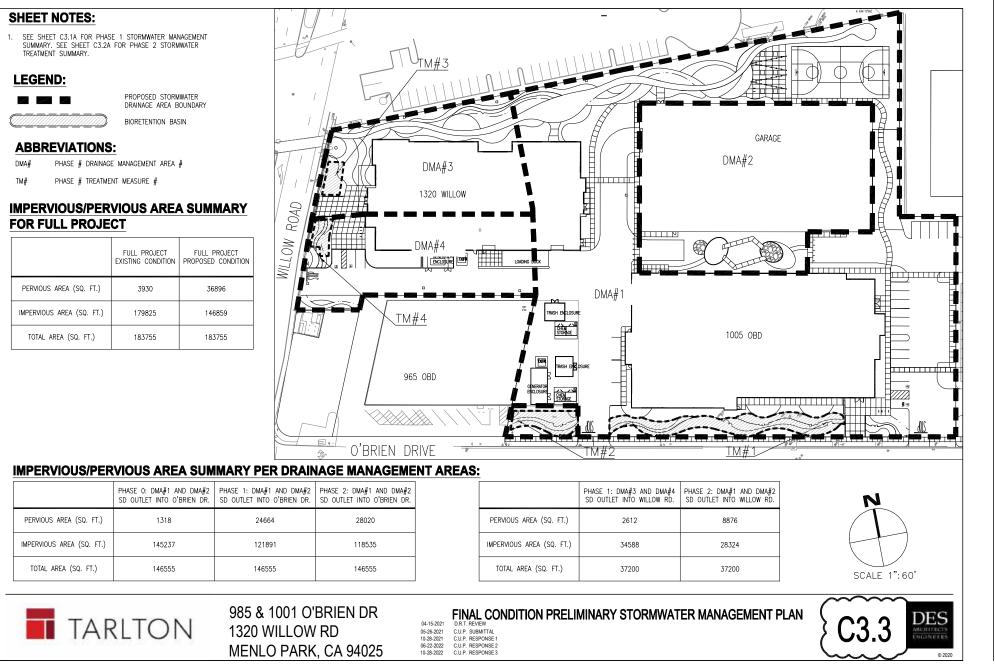


FIGURE 6 - PRELIMINARY OVERALL STORMWATER MANAGMENT PLAN DATED 01/06/2023

0.//Tariton - 1005 OBD/10025002_A_1005OBD_SHELL_2020_Central.

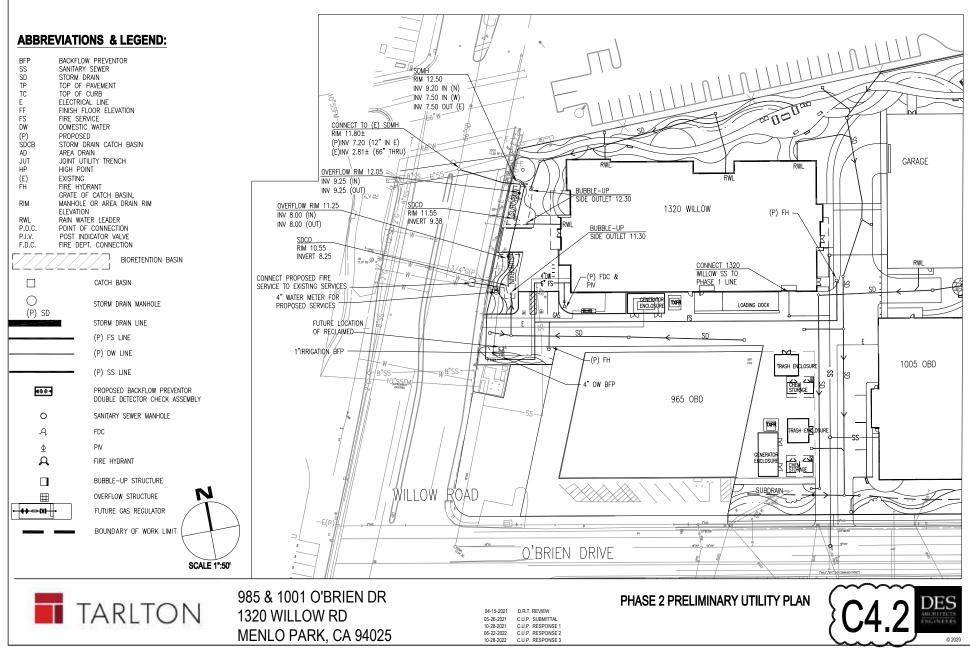
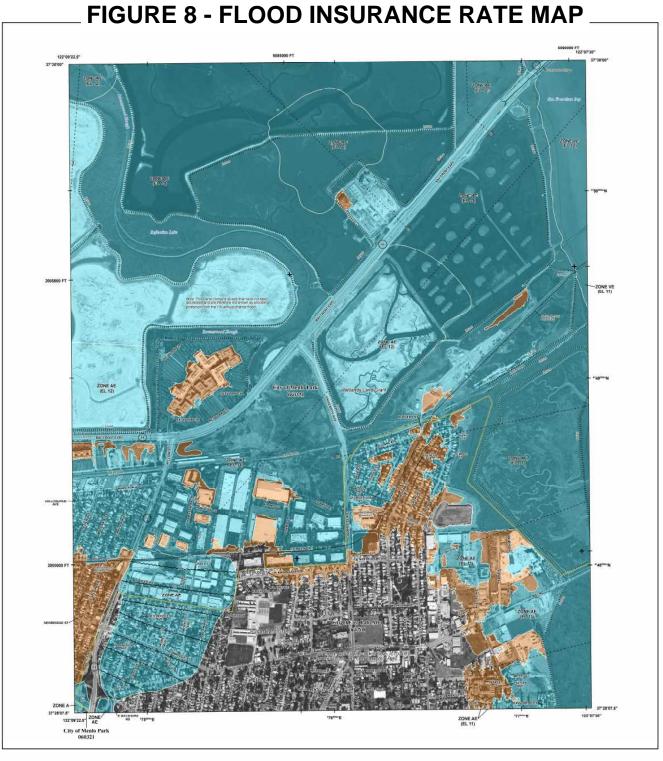
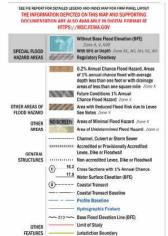


FIGURE 7 - PRELIMINARY PHASE 2 UTILITY PLAN DATED 01/25/2023

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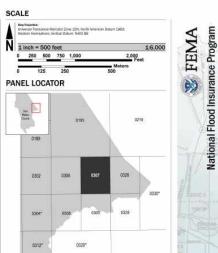
FLOOD HAZARD INFORMATION



NOTES TO USERS

For other space and a sectore state of the rough a soluble product a product with the PFM interfaced terms of entermarks and PFM interfaced terms of the PFM interfaced terms of the PFM interfaced terms of entermarks and the PFM interfaced terms of PFM interfaced terms of the interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the pFM interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the pFM interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the pFM interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the pFM interfaced terms of the interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the PFM interfaced terms of the interfaced terms of the PFM inter

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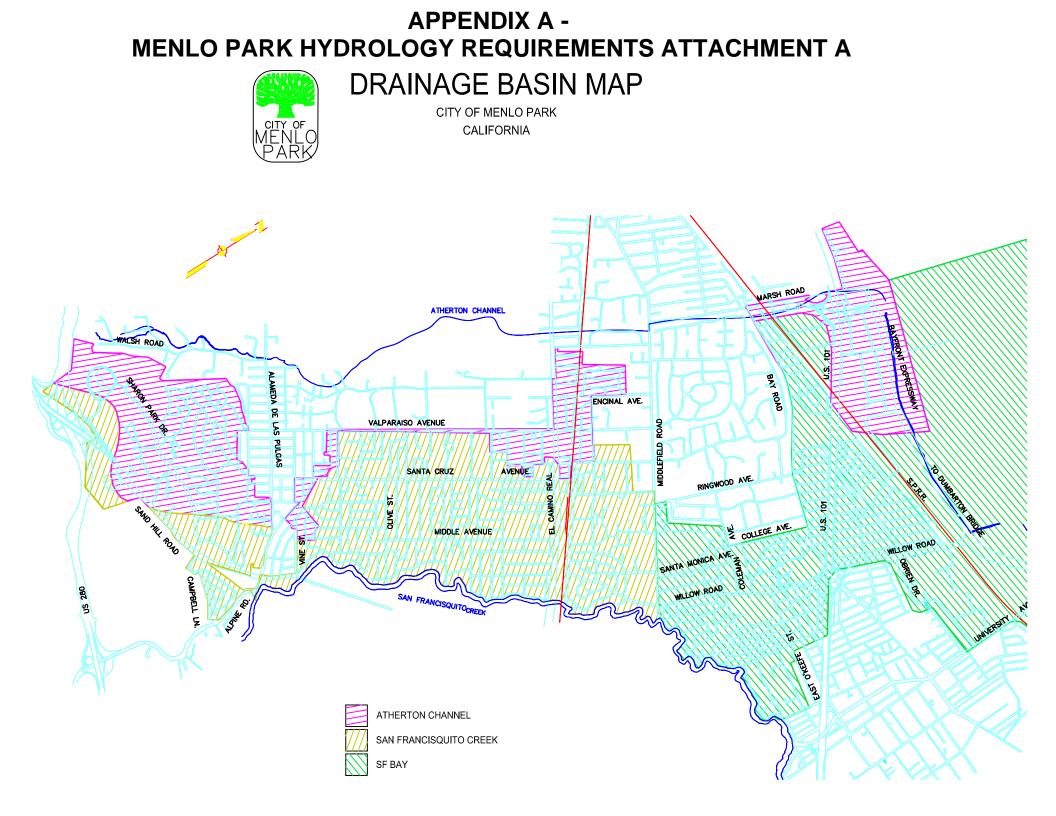


*PANEL NOT PRINTED

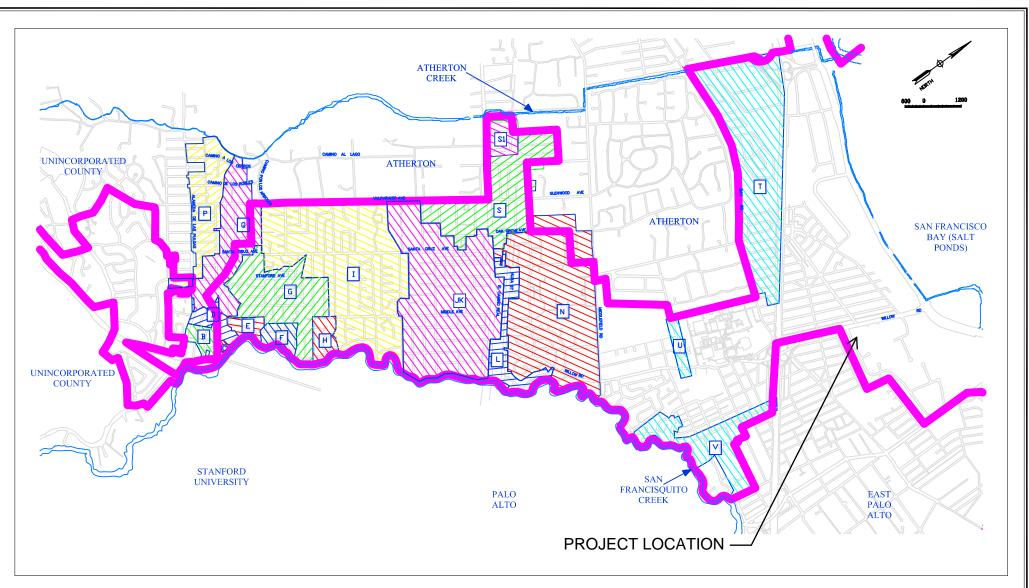




APPENDIX A: MENLO PARK HYDROLOGY REQUIREMENTS ATTACHMENTS A AND B



APPENDIX A -MENLO PARK HYDROLOGY REQUIREMENTS ATTACHMENT B





ATTACHMENT B STORM SYSTEM DRAINAGE AREAS MAP APPENDIX B: CITY OF MENLO PARK IMPERVIOUS AREA WORKSHEET

APPENDIX B

IMPERVIOUS AREA WORKSHEET Page 1

Submit this form with the improvement plan set to the City of Menlo Park Engineering Division.

Date: 01/06/23		,		<u>60; 055421050;</u>
Property Address: 13	20 Willow Road (P	hase 2): Sto	0554211 rm Drain Outle	
Project Description: N	ew Building and si	ite improvem	ients	
<u> </u>				
Contact Name: Diana	Rangel			
Contact Telephone N	umber: <u>650-364-6</u> 4	453		
Contact Email:drange	lr@des-ae.com			
Title And Sheet# of S	ubmitted Drawing us	sed For Calcu	lations: C3.2A	
Land Use (Circle One Residential		ndustrial	Professional	Roadway
Drainage Basin (Circle (See the <i>Hydrolog</i>	e One): y Report Requireme	ents for a Drair	nage Basin map	.)
Atherton Creek	San Francis	quito Creek	San Franci	isco Bay
I certify that the calcu impervious surfaces f		•	the proposed ch	nanges and final
Calculations Performe	ed By (Print): <u>Max E</u>	DeAndreis, P	'E	
	Title: <u>C</u>	ivil Engineer		
Calculations Performe	ed By (Signature): Date: <u>01</u>	Jolin Maji 1/06/23	und Other	úr _

APPENDIX B

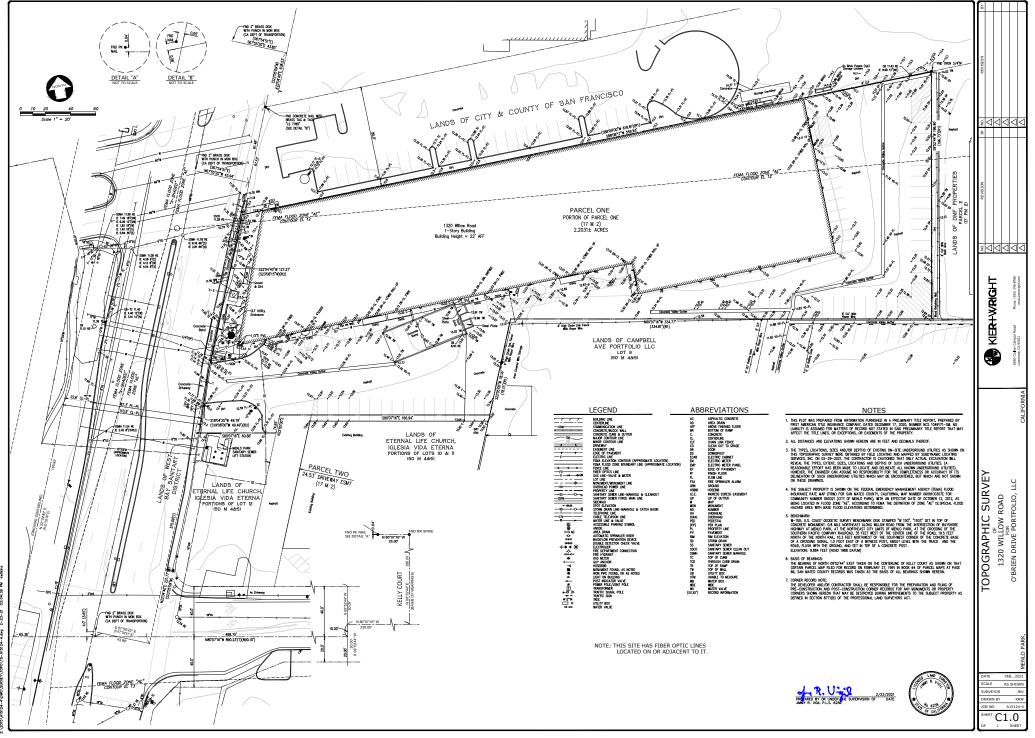
IMPERVIOUS AREA WORKSHEET Page 2

IMPERVIOUS AREA TABLE					
Total Area of Parcel		A <u>37200 ft²</u>			
Existing Pervious Area		B <u>2612 ft²</u>			
Existing Impervious Area		$\frac{c}{ft^2}$ 34588			
Existing % Impervious	$\frac{C}{A}$ x 100	D <u>92.9</u> %			
Existing Impervious Area To Be Replaced W/ New Impervious Area		E <u>ft²</u> 28324			
Existing Pervious Area To Be Replaced W/ New Impervious Area		\overline{F}_{ft^2} 0			
New Impervious Area (Creating and/or Replacing)* *If greater than 10,000sqft, a hydrology report must be submitted	E + F	G 28324 ft ²			
Existing Impervious Area To Be Replaced W/ New Pervious Area		H <u>6264</u> ft ²			
Net Change In Impervious Area ¹	F–H	I <u>ft²</u> -6264			
Proposed Pervious Area	B – I	$\begin{array}{c c} \overline{J} \\ \overline{ft^2} & 8876 \end{array}$			
Proposed Impervious Area* *Verify that J + K = A	C + I	Κ <u>ft²</u> 28324			
Proposed % Impervious	$\frac{K}{A}$ x 100	L <u>%</u> 76.1			

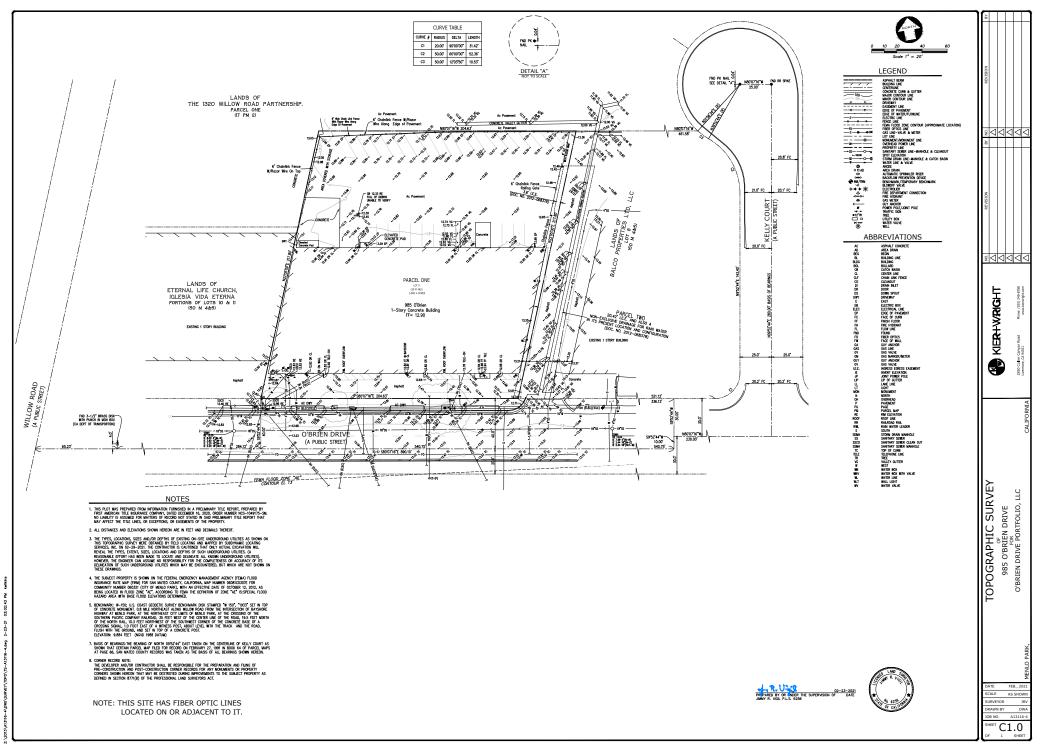
¹ Net change in impervious area is the area required by

APPENDIX C:

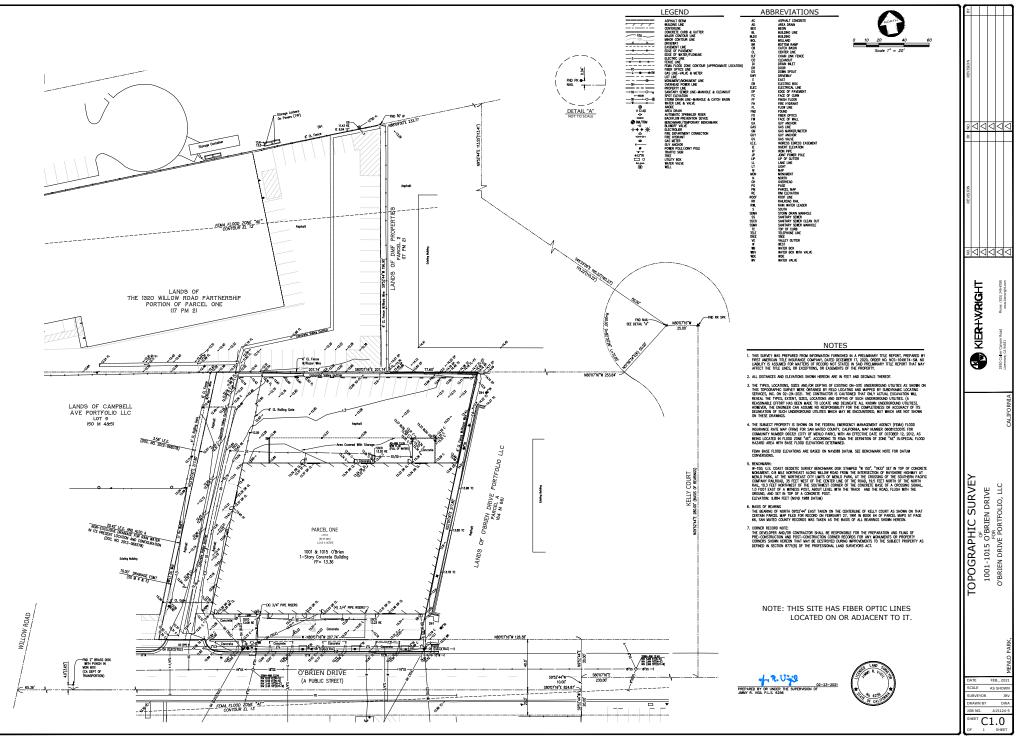
EXISTING CONDITIONS TOPOGRAPHIC SURVEY



APPENDIX C - EXISTING CONDITIONS AND TOPOGRAPHIC SURVEY



APPENDIX C - EXISTING CONDITIONS AND TOPOGRAPHIC SURVEY



APPENDIX C - EXISTING CONDITIONS AND TOPOGRAPHIC SURVEY